

Non-linear Effects in Physics of Dielectrics

DIELECTRIC TUTORIAL

*Madrid, Spain
6 September 2010*

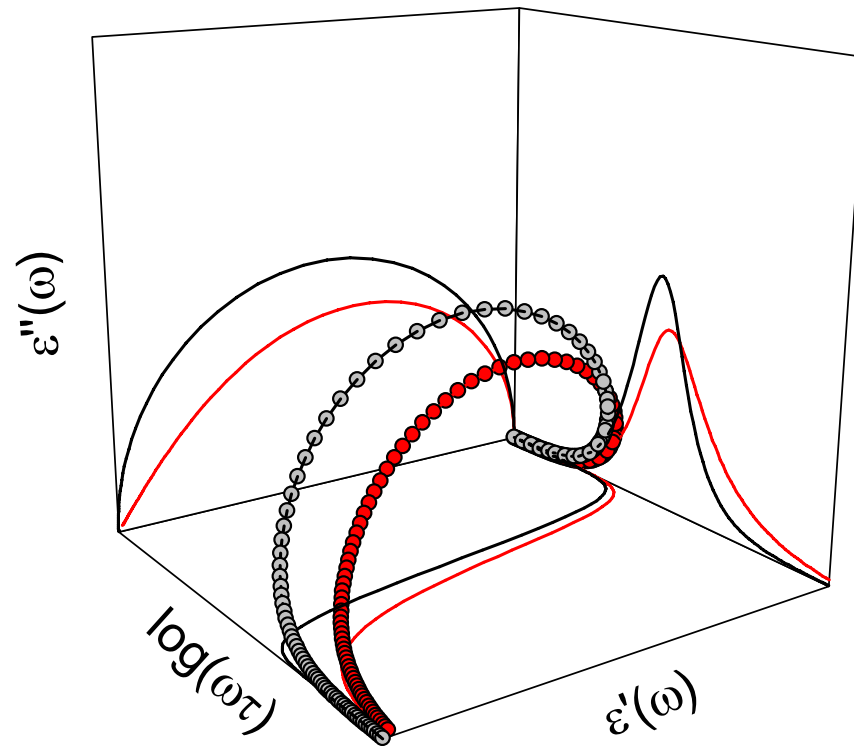
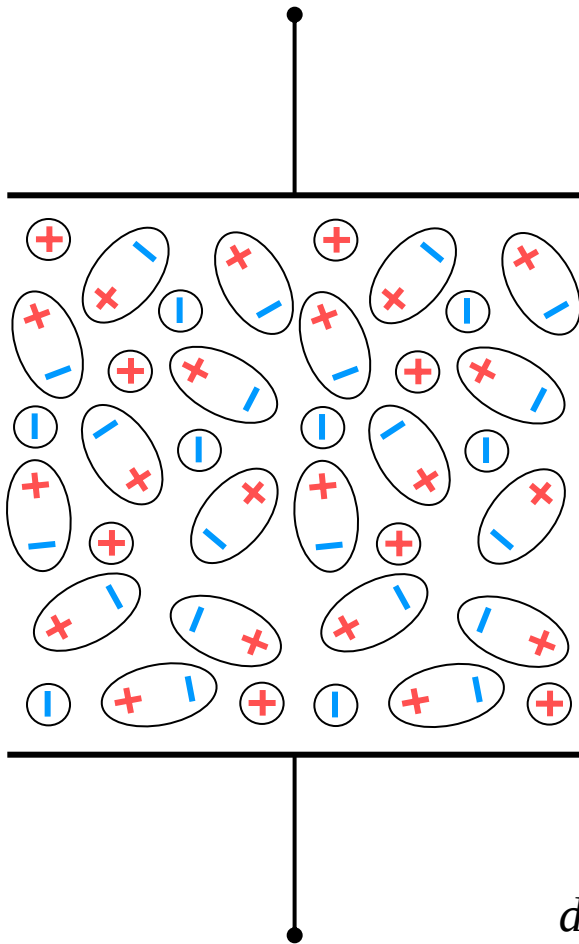
High-Field Dielectric Response:

- ▶ Coulombic stress
- ▶ Langevin effect
- ▶ Energy absorption
- ▶ Time-resolved technique
- ▶ Reverse isothermal calorimetry

Ranko Richert

dielectric relaxation technique

$$\mathbf{D} = \epsilon \epsilon_0 \mathbf{E}$$

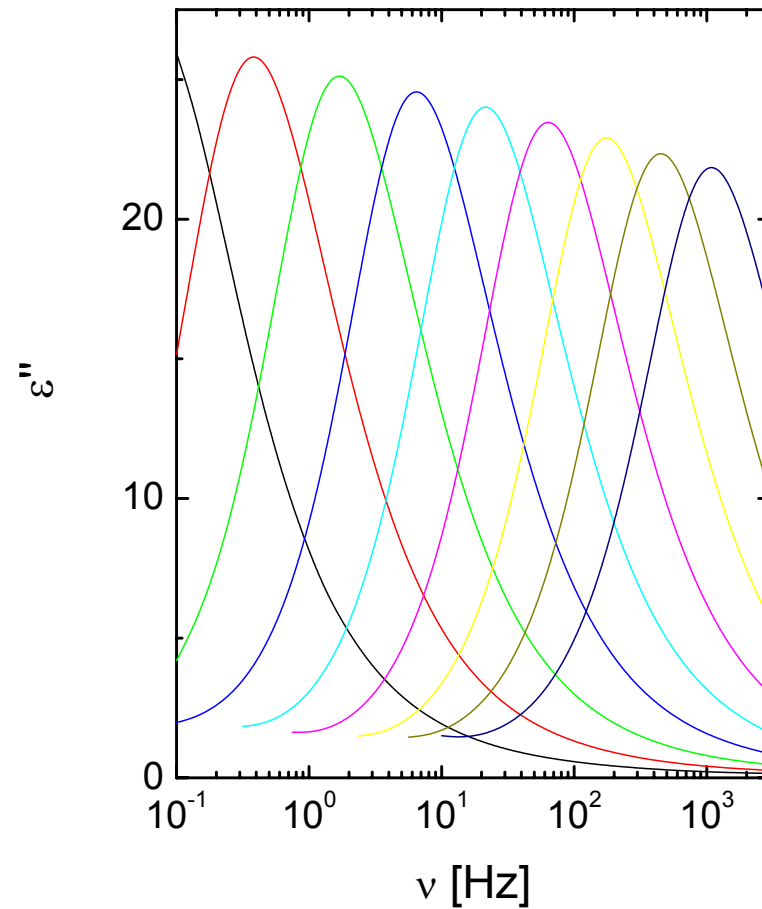
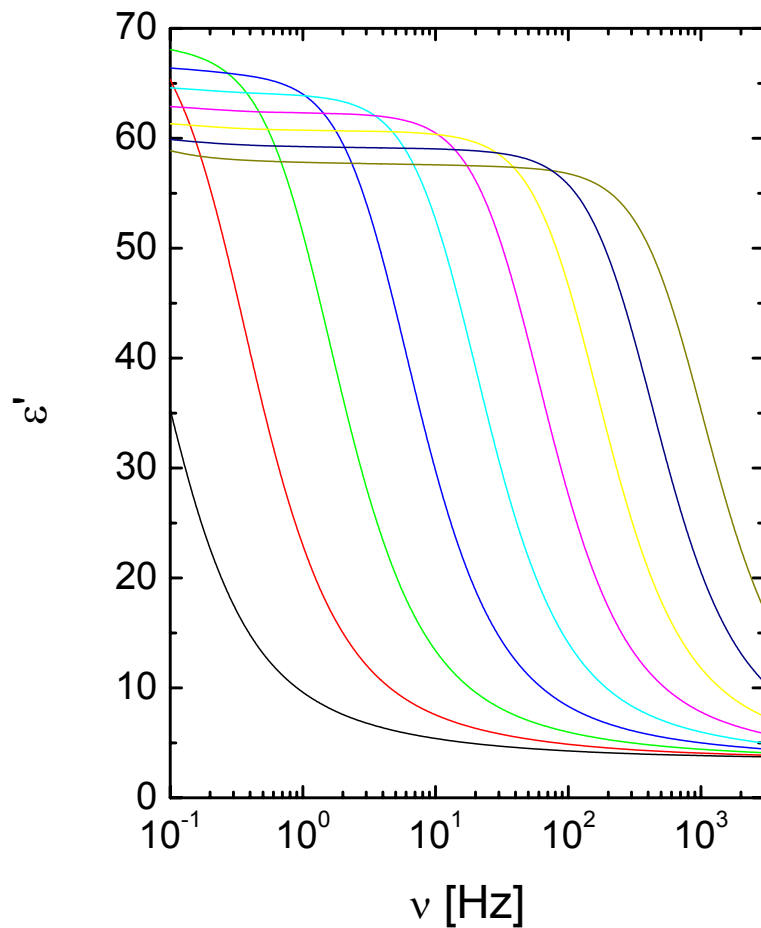


dielectric
displacement

$$\mathbf{D} \equiv \frac{\mathbf{Q}}{\mathbf{A}} \propto \frac{\mathbf{V}}{\mathbf{d}} \equiv \mathbf{E} \quad \text{electric field}$$

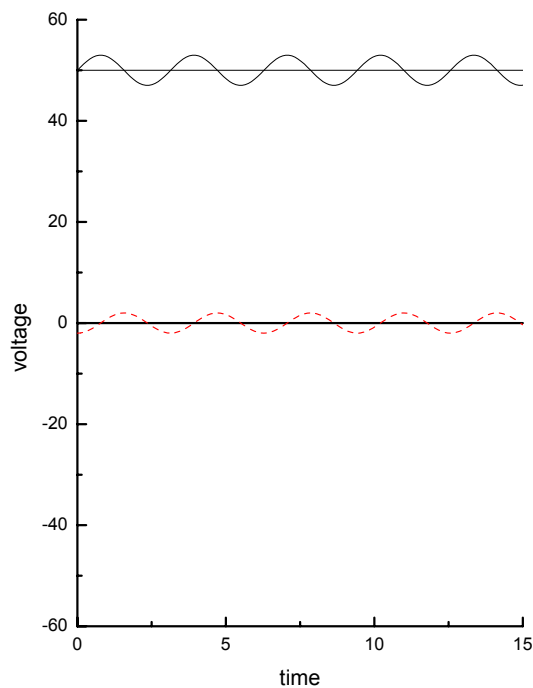
typical case near the glass transition

propylene glycol $T = 174 - 198 \text{ K}$ (3 K)



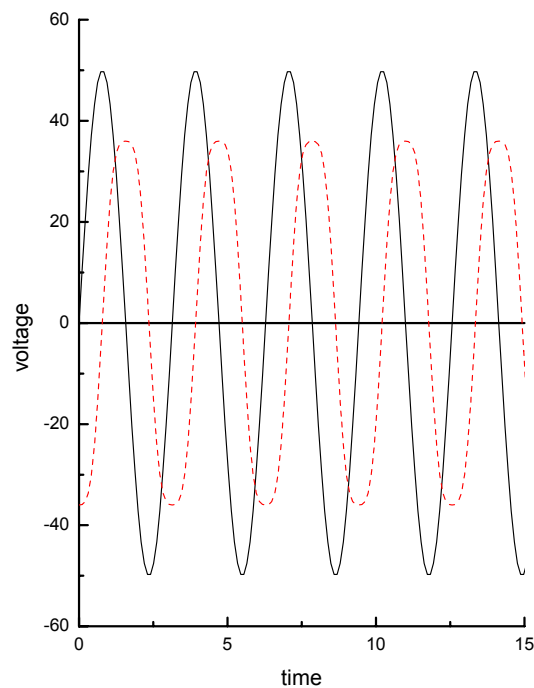
result usually independent of field amplitude

variety of high field techniques

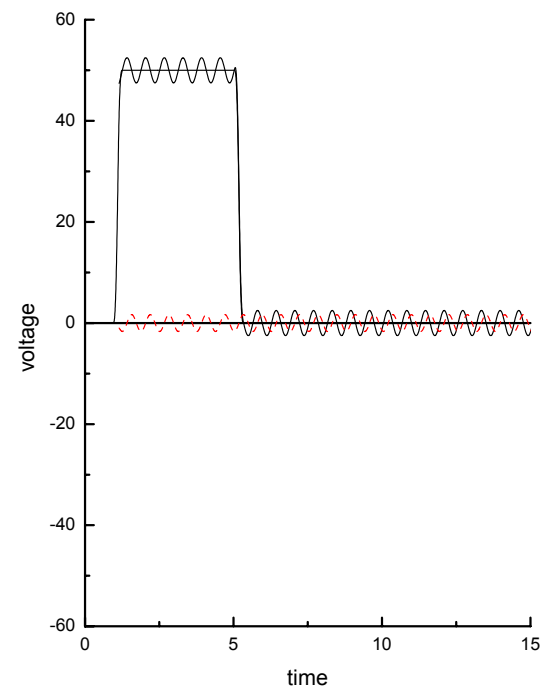


high DC field
low AC field
mainly 1ω

Heats via σ_{dc}



high AC field
no bias
 $1\omega + 3\omega$



low AC field
on high pulse
NDE(t)

avoid heating

non-linear susceptibility

$$\frac{\mathbf{P}}{\varepsilon_0} = \underbrace{\chi^{electret}}_{\substack{=0 \\ \text{causality}}} + \chi \mathbf{E} + \underbrace{\chi^{(1)} \mathbf{E} \mathbf{E}}_{\substack{=0 \\ \text{symmetry}}} + \chi^{(2)} E^2 \mathbf{E} + \underbrace{\chi^{(3)} E^3 \mathbf{E}}_{\substack{=0 \\ \text{symmetry}}} + \chi^{(4)} E^4 \mathbf{E} + \dots$$

causality: $\mathbf{P}(0) = 0$

symmetry: $\mathbf{P}(\mathbf{E}) = -\mathbf{P}(-\mathbf{E})$

$$\frac{\mathbf{P}}{\varepsilon_0 \mathbf{E}} = \chi + \chi^{(2)} E^2 + \chi^{(4)} E^4 + \dots$$

$$\varepsilon_s(E^2) = \varepsilon_s(0) \times [1 - \lambda E^2]$$

$$\lambda = -\Delta \ln(\varepsilon_s) / E^2$$

Piekara factor :

$$\Delta \varepsilon_s / E^2 = -\lambda \varepsilon_s$$

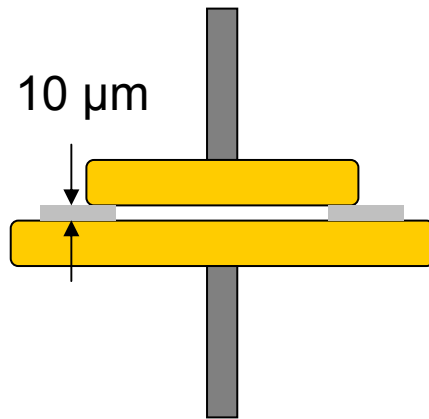
~~$$\text{superposition principle : } P(t) = \int_{-\infty}^t dP(\theta) = \chi \varepsilon_0 \int_{-\infty}^t E(\theta) \varphi(t - \theta) d\theta$$~~

M. S. Green, R. Kubo (1950's) : linear transport coefficients $L_{F_e=0}$ are related to auto - correlation function of the equilibrium fluctuations in the conjugate flux J

~~$$J = L_{F_e=0} F_e \qquad L_{F_e=0} = \frac{V}{kT} \int_0^\infty \langle J(0) J(t) \rangle_{F_e=0} dt$$~~

Coulombic stress

Coulombic stress exercise



top electrode 16 mm Ø
 bottom electrode 30 mm Ø
 ring outer: 20 mm Ø
 ring inner: 14 mm Ø

glycerol at $E_0 = 283$ kV/cm

$$\text{work } Fd = \text{energy } \frac{1}{2} QV$$

$$F \partial d = \frac{1}{2} \partial(QV) = \underbrace{\frac{1}{2} Q \partial V}_{=0} + \frac{1}{2} V \partial Q =$$

$$\frac{1}{2} V \partial(CV) = \underbrace{\frac{1}{2} VC \partial V}_{=0} + \frac{1}{2} V^2 \partial C = \frac{1}{2} V^2 \epsilon_0 A \partial d^{-1}$$



$$F(t) = \frac{\epsilon_s \epsilon_0 A}{2} E^2(t) = \frac{\epsilon_s \epsilon_0 A}{4} E_0^2 \times [1 - \cos(2\omega t)]$$

$$\Delta \ln \epsilon = -\frac{\Delta d}{d} = +\frac{F_0}{aY} = \frac{\epsilon_s \epsilon_0 A}{4aY} E_0^2$$

$$a = 4.7 \times 10^{-5} \text{ m}^2 \text{ (Teflon ring, } d = 14 - 16 \text{ mm)}$$

$$Y > 1 \text{ GPa (Teflon only)}$$

$$F_0 = 31 \text{ N}$$

$$F_0/a = 0.67 \text{ MPa}$$

$$\Delta \ln \epsilon = -\frac{\Delta d}{d} \leq 6.7 \times 10^{-4}$$

dielectric saturation

expected non-linearity: dielectric saturation (aka Langevin effect)

$$\langle \cos \theta \rangle = \frac{\int_0^\pi \cos \theta e^{\mu E \cos \theta / kT} d\theta}{\int_0^\pi e^{\mu E \cos \theta / kT} d\theta} \Rightarrow$$

$$\langle \cos \theta \rangle = \coth\left(\frac{\mu E}{kT}\right) - \left(\frac{\mu E}{kT}\right)^{-1}$$

$$\langle \cos \theta \rangle = L\left(\frac{\mu E}{kT}\right) \quad \left(\begin{array}{l} \text{Langevin} \\ \text{function} \end{array} \right)$$

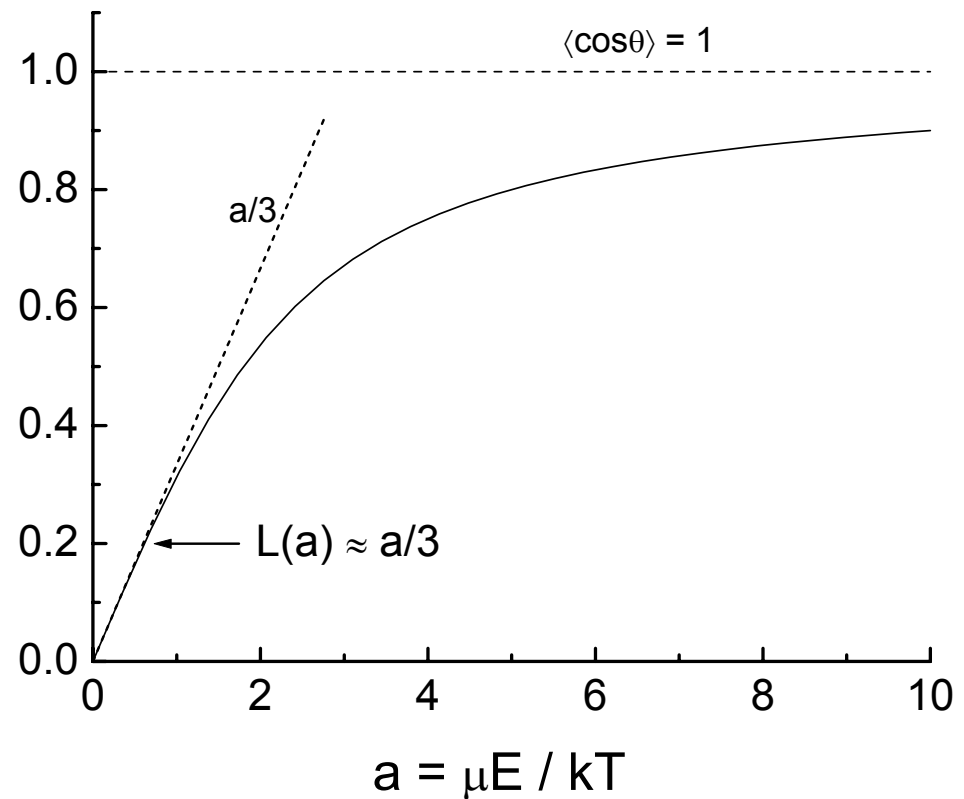
$$\text{with } a = \frac{\mu E}{kT}$$

$$\langle \cos \theta \rangle = L(a) = \coth(a) - \frac{1}{a}$$

if $\mu E \ll kT$ or $a \ll 1$

$$\langle \cos \theta \rangle \approx \frac{a}{3} = \frac{\mu E}{3kT}$$

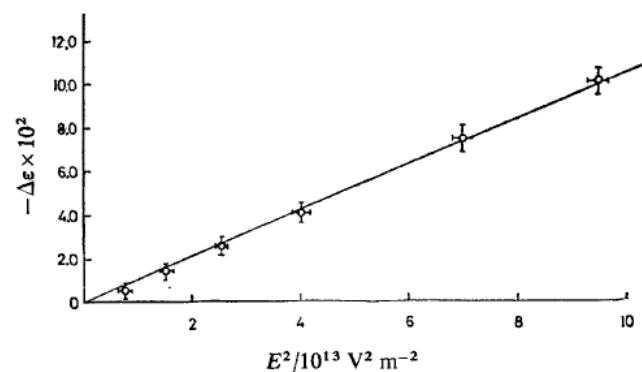
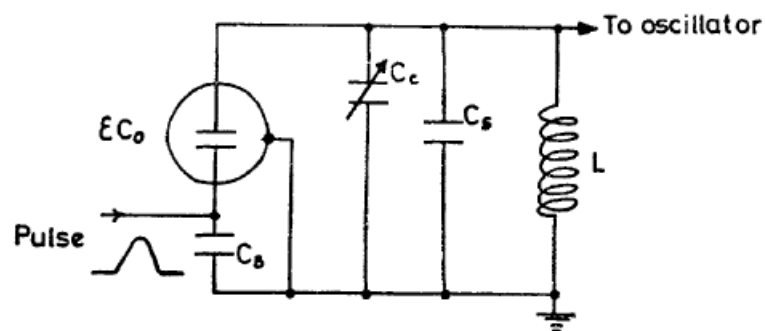
$L(a) = \langle \cos \theta \rangle$



saturation in water at 293 K

Piekara $\Delta\epsilon_s/E^2 = -\lambda\epsilon_s$

vanVleck
$$\frac{\Delta\epsilon_s}{E^2} = \frac{\epsilon_s(E^2) - \epsilon_s(0)}{E^2} = -\frac{N\mu^4}{45\epsilon_0 V(kT)^3} \times \frac{\epsilon_s^4(\epsilon_\infty + 2)^4}{(2\epsilon_s + \epsilon_\infty)^2(2\epsilon_s^2 + \epsilon_\infty^2)}$$



H. A. Kolodziej, G. Parry Jones, M. Davies, J. Chem. Soc. Faraday Trans. 2 71 (1975) 269

J. H. van Vleck, J. Chem. Phys. 5 (1937) 556

A. Piekara, Acta Phys. Polon. 18 (1959) 361

time resolved NDE experiments

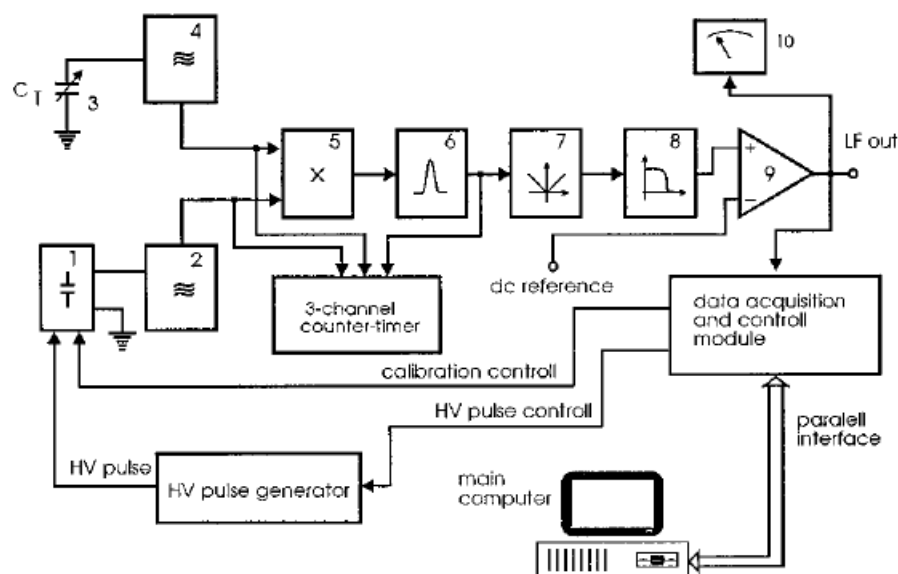
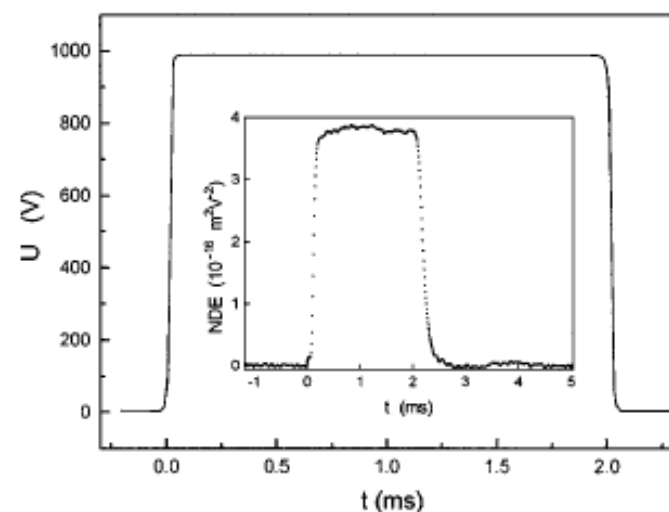
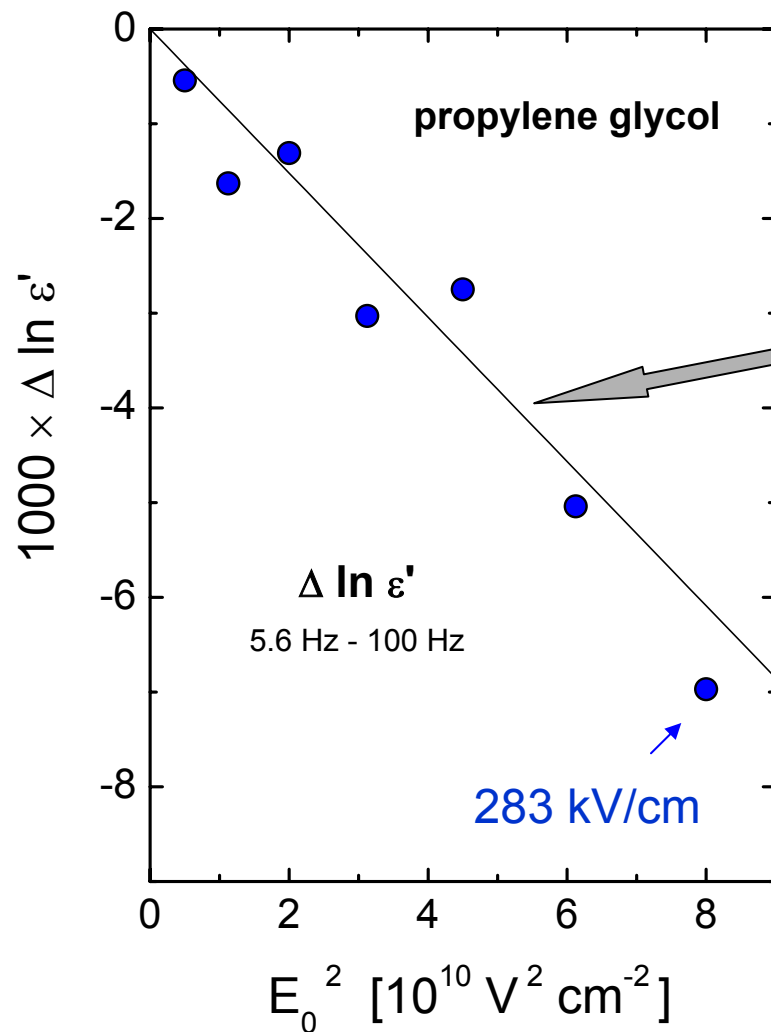


FIG. 1. The NDE measurement setup: 1—Measurement capacitor; 2—measurement generator (G_1 , freq. $f_1 + \Delta f$); 3,4—reference generator (G_2 , freq. f_2) with tuning capacitor; 5—mixer (freq. Δf); 6—bandpass filter; 7—rectifier; 8—low-pass filter; 9—amplifier; 10—indicator of the tuning of G_2 to $f_2 = f_1 + \Delta f$. The elements 2 and 4–10 are contained in one measurement unit.



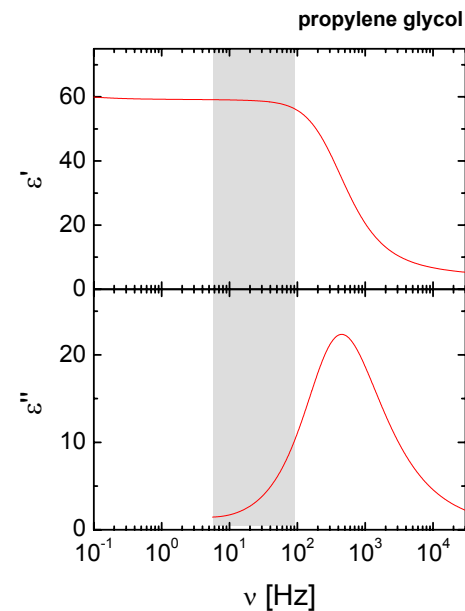
field effect (71 - 283 kV/cm) result for propylene glycol



$$\langle \cos \theta \rangle = \frac{\int_0^\pi \cos \theta e^{\mu E \cos \theta / kT} d\theta}{\int_0^\pi e^{\mu E \cos \theta / kT} d\theta} \approx \frac{\mu E}{3kT} \leq 1$$

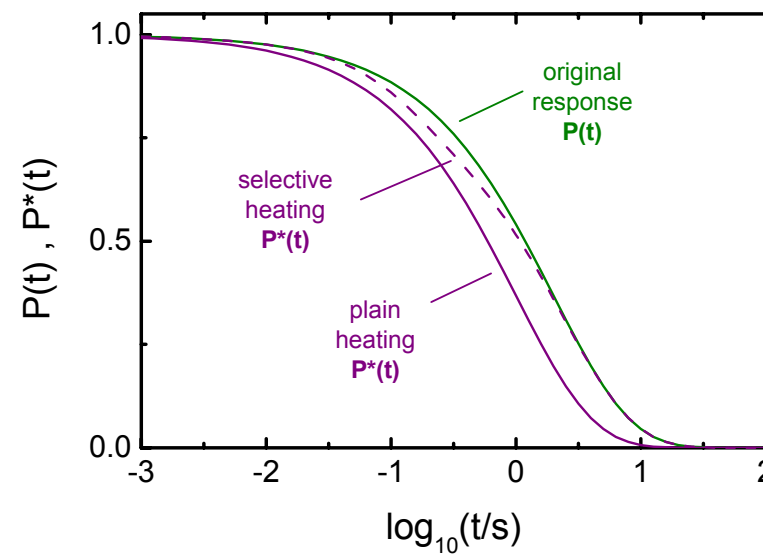
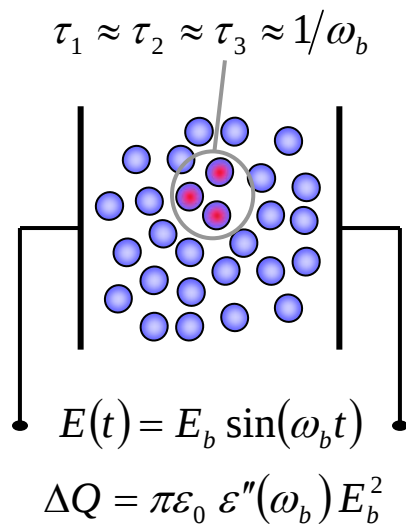
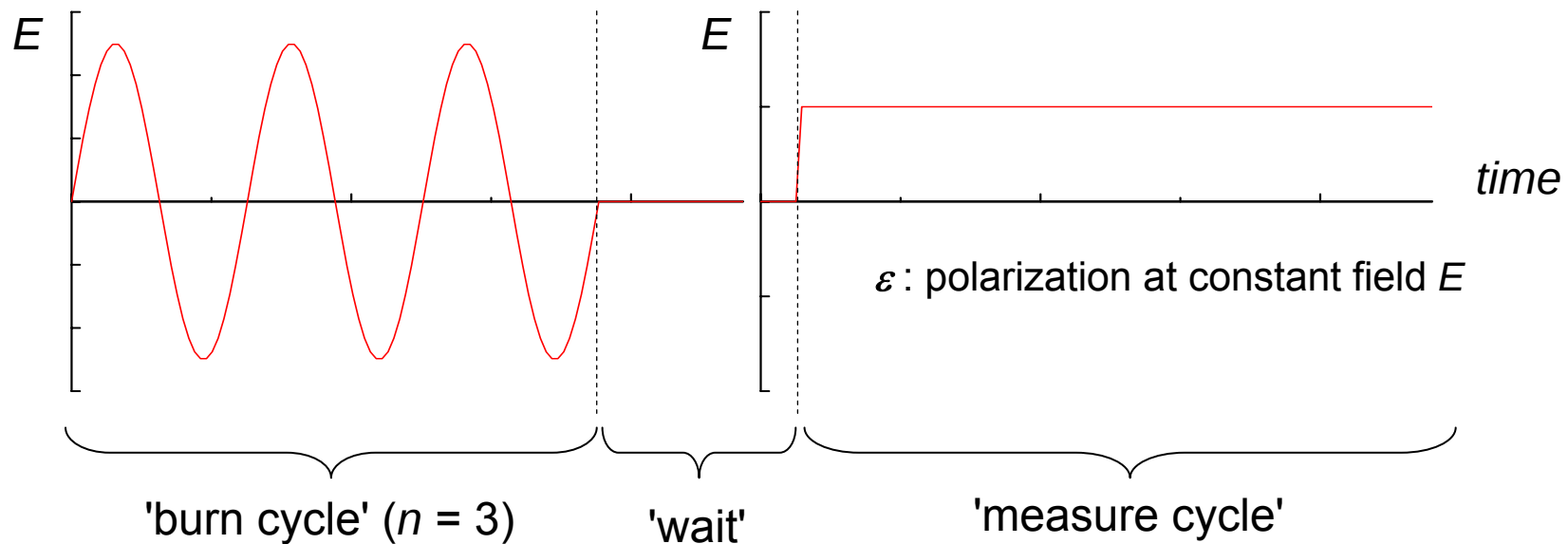
$$\frac{\Delta \epsilon_s}{E^2} = -\frac{N\mu^4}{45\epsilon_0 V(kT)^3} \times \frac{\epsilon_s^4 (\epsilon_\infty + 2)^4}{(2\epsilon_s + \epsilon_\infty)^2 (2\epsilon_s^2 + \epsilon_\infty^2)}$$

(van Vleck)



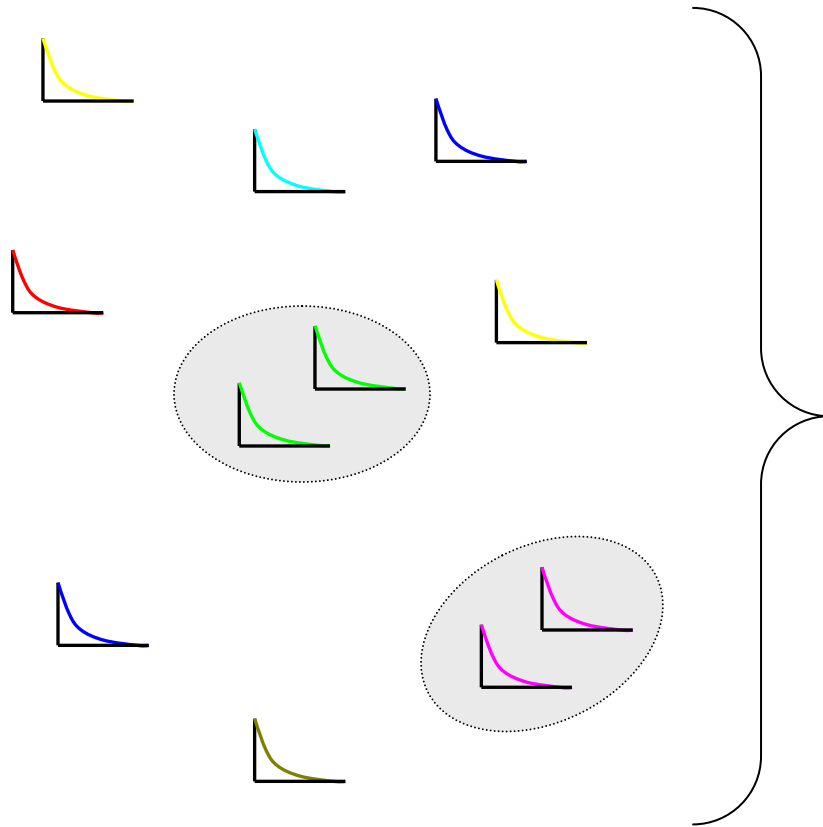
energy absorption

dielectric hole-burning technique: summary

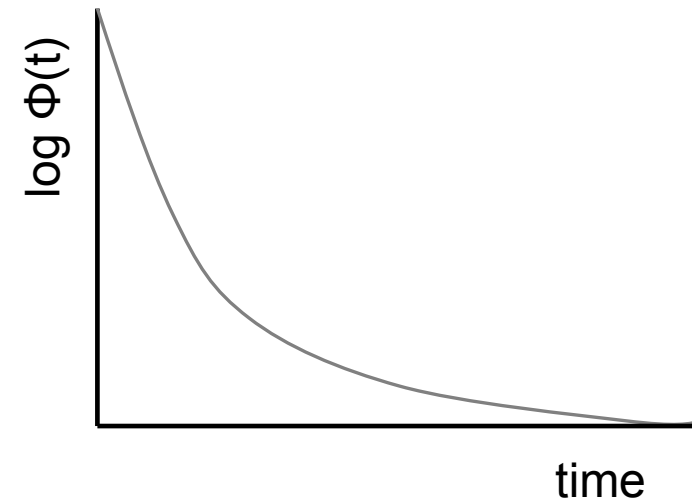


features of homogeneous dynamics

local behavior

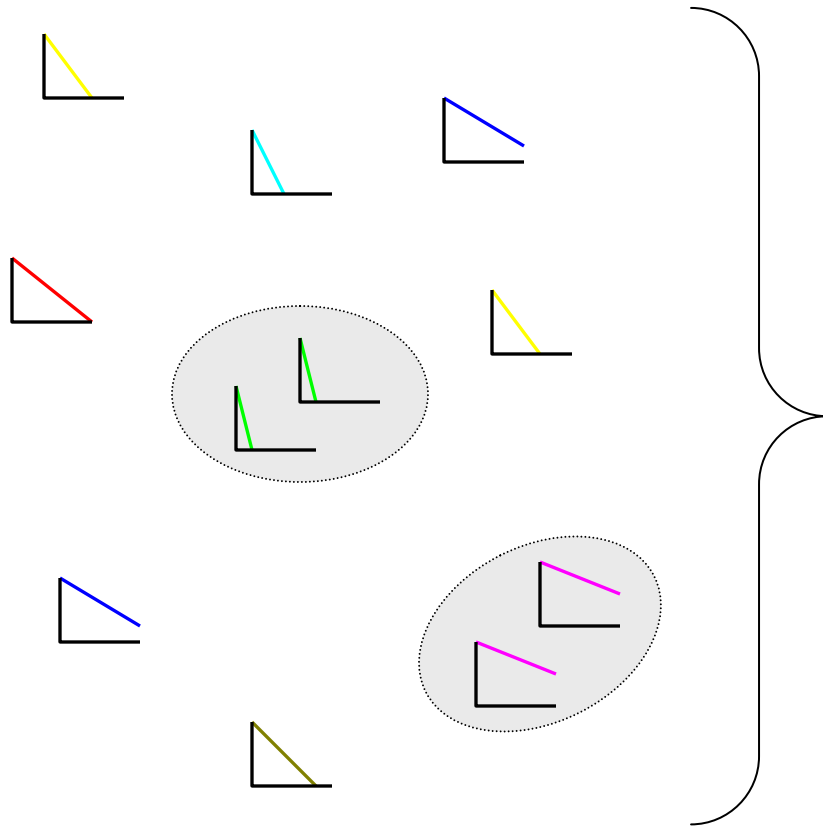


ensemble average

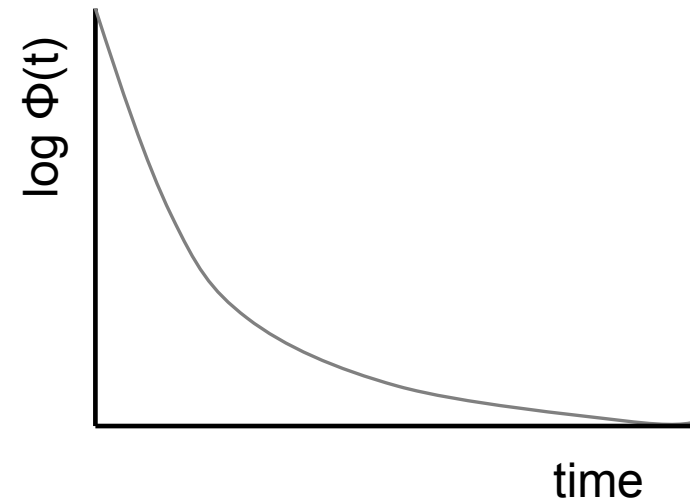


features of heterogeneous dynamics

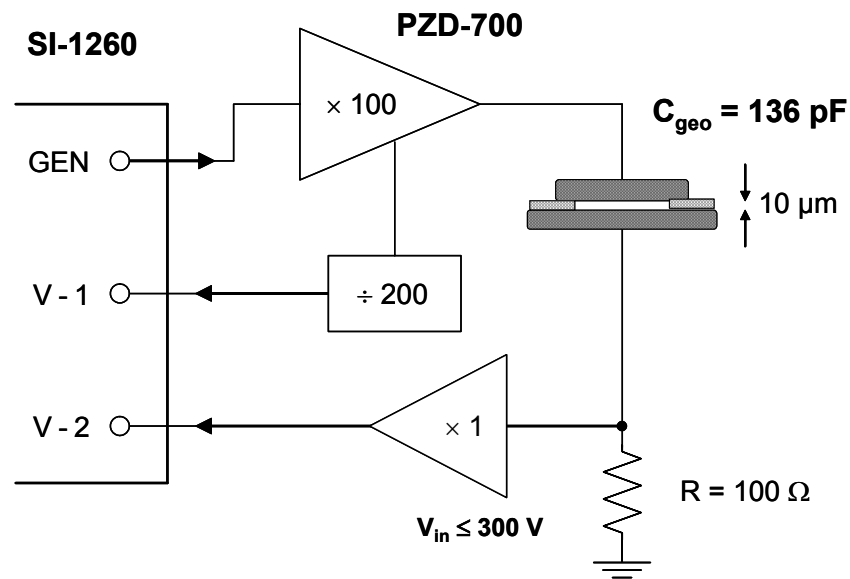
local behavior



ensemble average



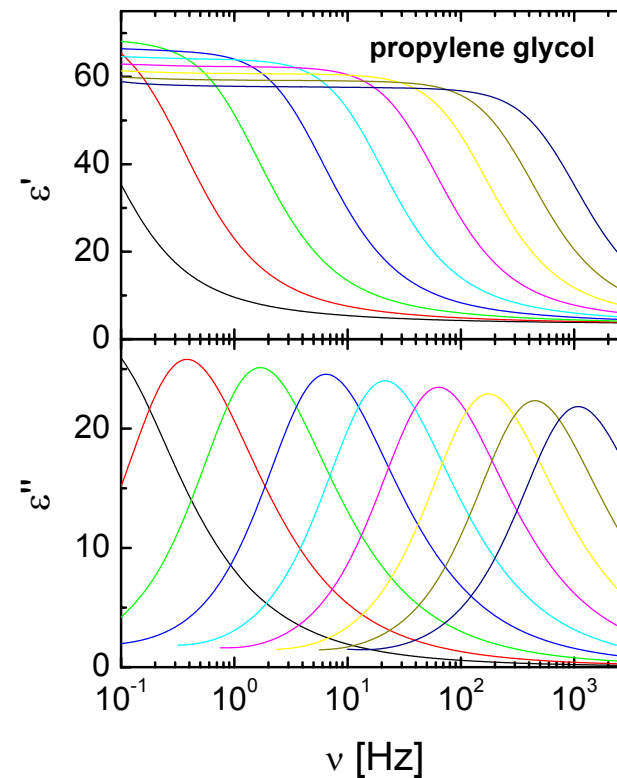
high field impedance - beyond the linear regime



fields up to 450 kV/cm

μE up to 0.082 kT

0.1 Hz to 50 kHz range



$$\frac{\mathbf{P}}{\epsilon_0} = \underbrace{\chi^{electret}}_{=0 \text{ causality}} + \underbrace{\chi \mathbf{E}}_{\uparrow} + \underbrace{\chi^{(1)} \mathbf{E} \mathbf{E}}_{=0 \text{ symmetry}} + \underbrace{\chi^{(2)} \mathbf{E}^2 \mathbf{E}}_{\text{usually too small}} + \underbrace{\chi^{(3)} \mathbf{E}^3 \mathbf{E}}_{=0 \text{ symmetry}} + \underbrace{\chi^{(4)} \mathbf{E}^4 \mathbf{E}}_{\text{usually way too small}} + \dots$$

analyzer input protection



Ultralow, Input-Bias Current
Operational Amplifier

AD549

AD 549 L

$$R_{in} = 10^{15} \Omega$$

$$C_{in} = 0.8 \text{ pF}$$

$$I_{bias} = 40 \text{ fA}$$

In the corresponding version of this scheme for a follower, shown in Figure 38, R_P and the capacitance at the positive input terminal produce a pole in the signal frequency response at a $f = 1/2\pi RC$. Again, the Johnson noise, R_P , adds to the amplifier's input voltage noise.

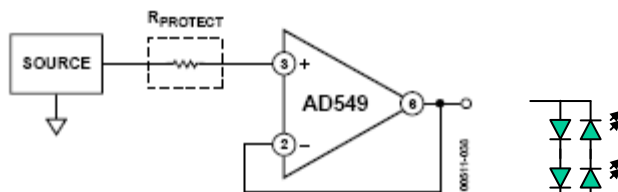
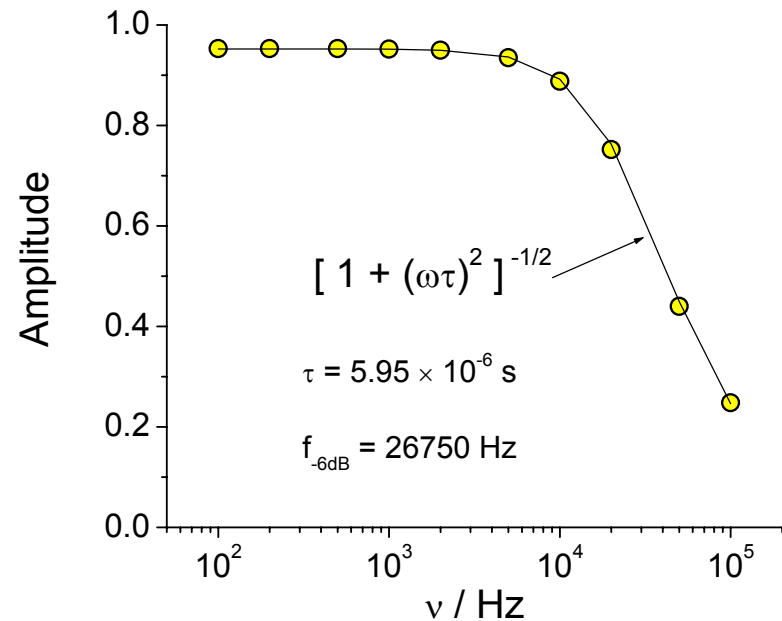
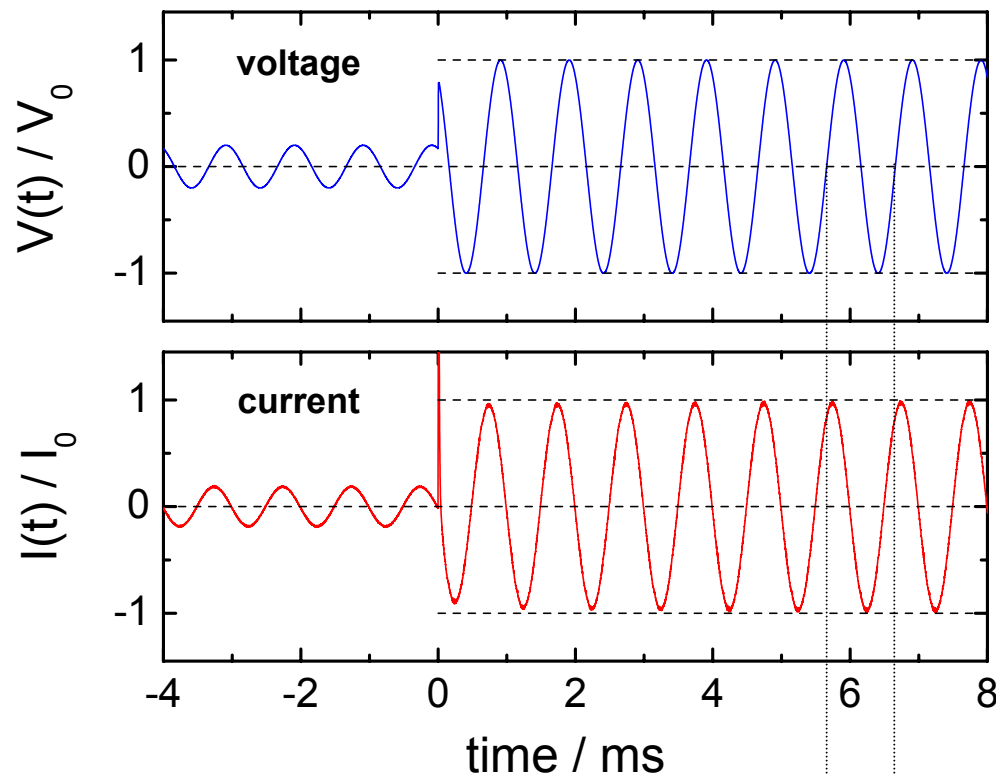
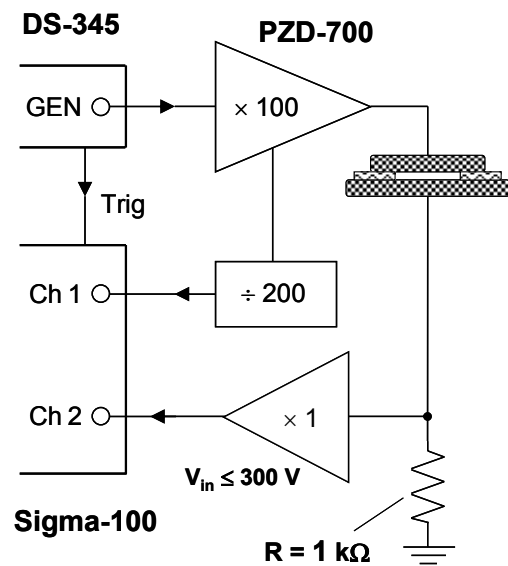


Figure 38. Follower with Input Current Limit



$R_{\text{PROTECT}} = 3 \text{ M}\Omega$:
protects against 300 V (no time limit)

adding time-resolution capabilities to high-field technique



field amplitude $\times 5$:
32.4 to 162 kV/cm

$$S(t) = V(t) \text{ or } I(t)$$

$$R = \frac{\omega}{\pi} \int_0^{2\pi/\omega} \sin(\omega t) S(t) dt = A \cos(\varphi)$$

$$I = \frac{\omega}{\pi} \int_0^{2\pi/\omega} \cos(\omega t) S(t) dt = A \sin(\varphi)$$

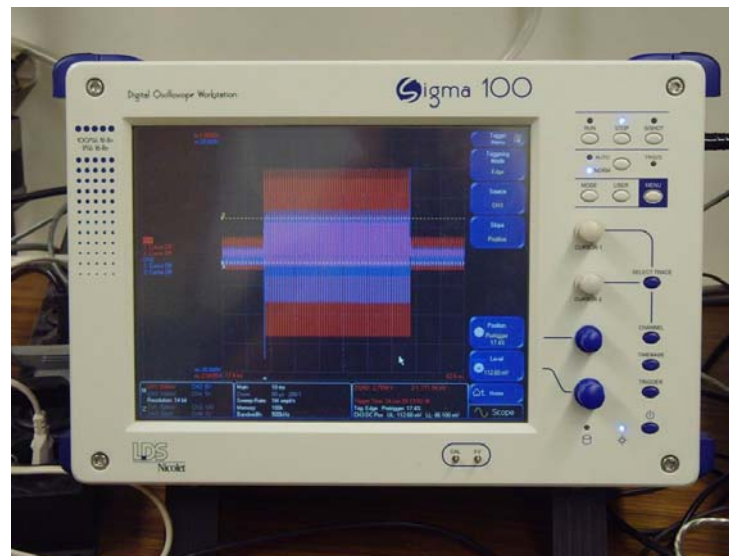
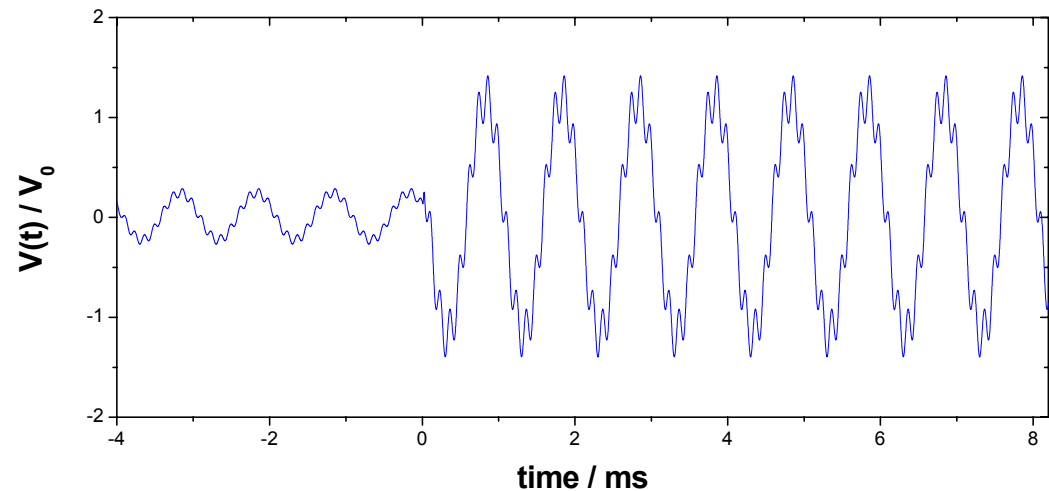
$$A = \sqrt{R^2 + I^2} \quad \varphi = \arctan\left(\frac{I}{R}\right)$$

$$\tan \delta = \tan\left(\frac{\pi}{2} - \Delta\varphi\right)$$

single / multiple frequency technique



Stanford Research DS-345 Generator



Nicolet Sigma 100 Digital Oscilloscope

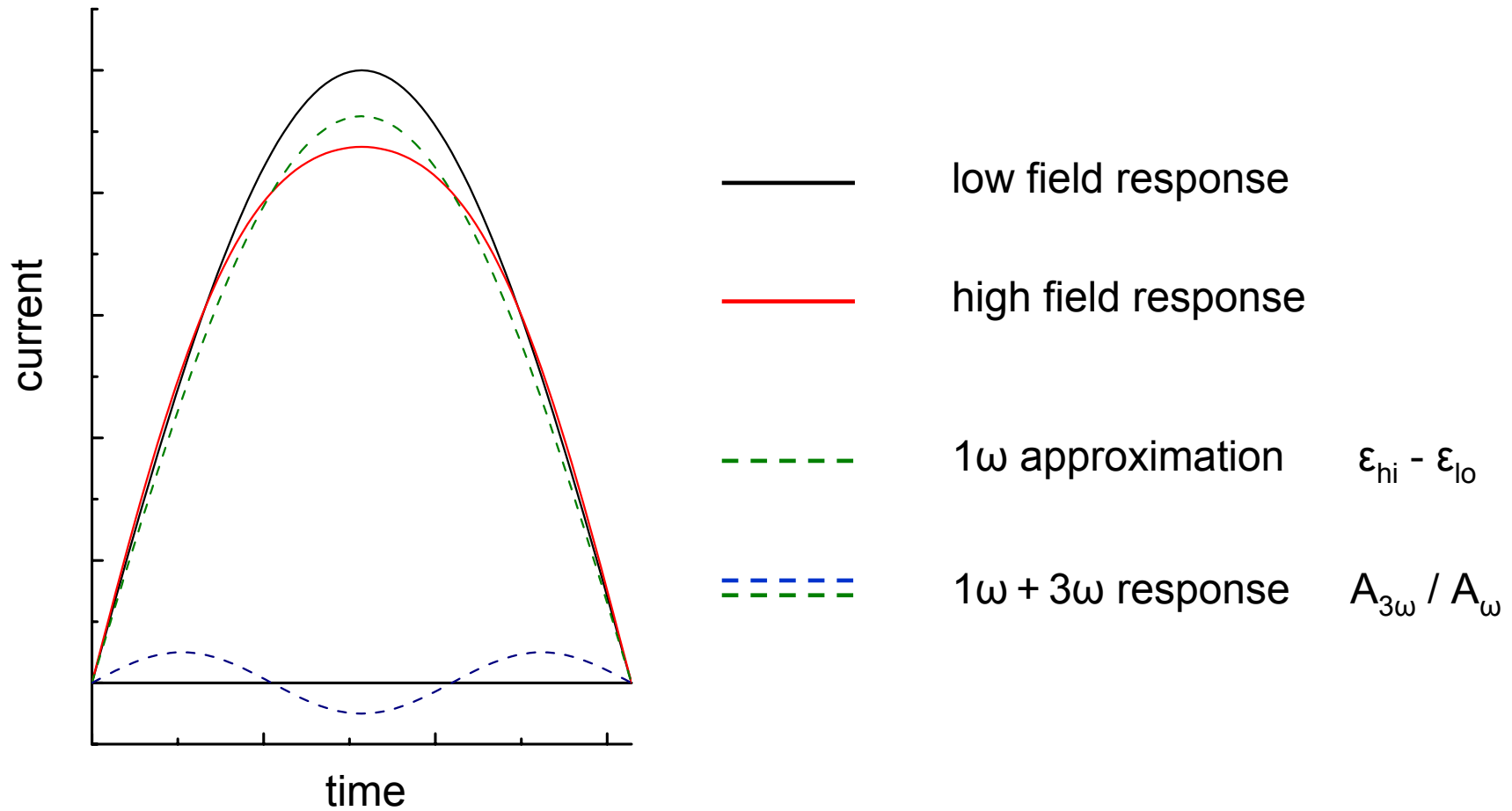
4 channels

1 Ms depth

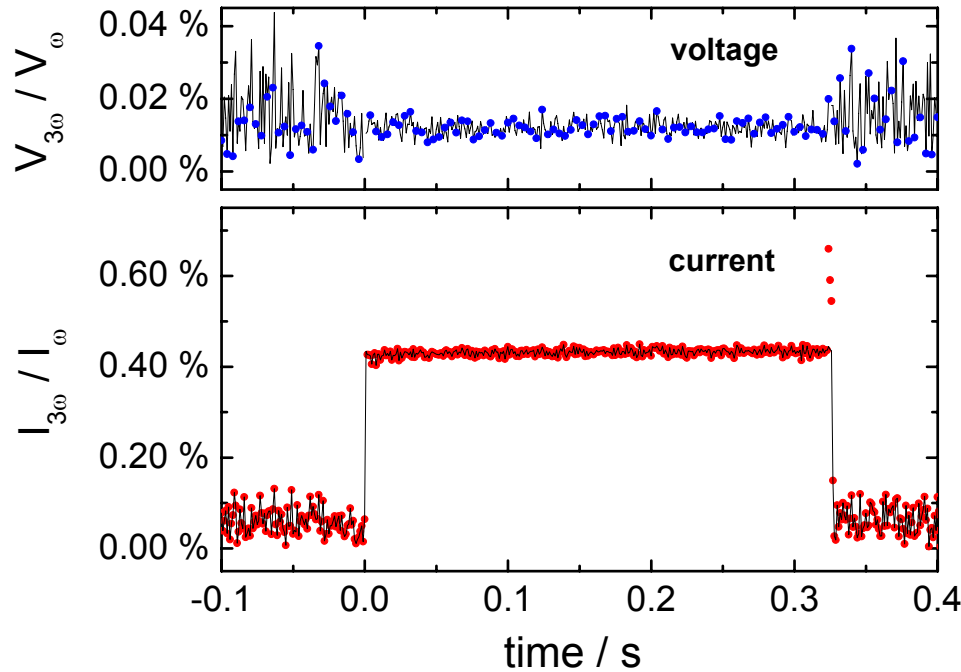
12 bit @ 100 Ms/s

14 bit @ 1 Ms/s

1 ω versus 3 ω data analysis



3 ω signal during field change: 32.4 to 162 kV/cm



$$\left. \begin{aligned} R &= \frac{\omega}{\pi} \int_0^{2\pi/\omega} \sin(3\omega t) V(t) dt \\ I &= \frac{\omega}{\pi} \int_0^{2\pi/\omega} \cos(3\omega t) V(t) dt \end{aligned} \right\} A = \sqrt{R^2 + I^2}$$

$$\begin{aligned} D_0 &= \varepsilon \varepsilon_0 E_0 + \lambda \varepsilon \varepsilon_0 E_0^3 \\ &= \varepsilon \varepsilon_0 E_0 \times (1 + \lambda E_0^2) \\ \lambda &= \Delta \ln \varepsilon / E_0^2 \end{aligned}$$

$$E = E_0 \sin(\omega t)$$

$$D_\omega(t) = \varepsilon \varepsilon_0 E_0 \sin(\omega t) + \lambda \varepsilon \varepsilon_0 E_0^3 \frac{3}{4} \sin(\omega t)$$

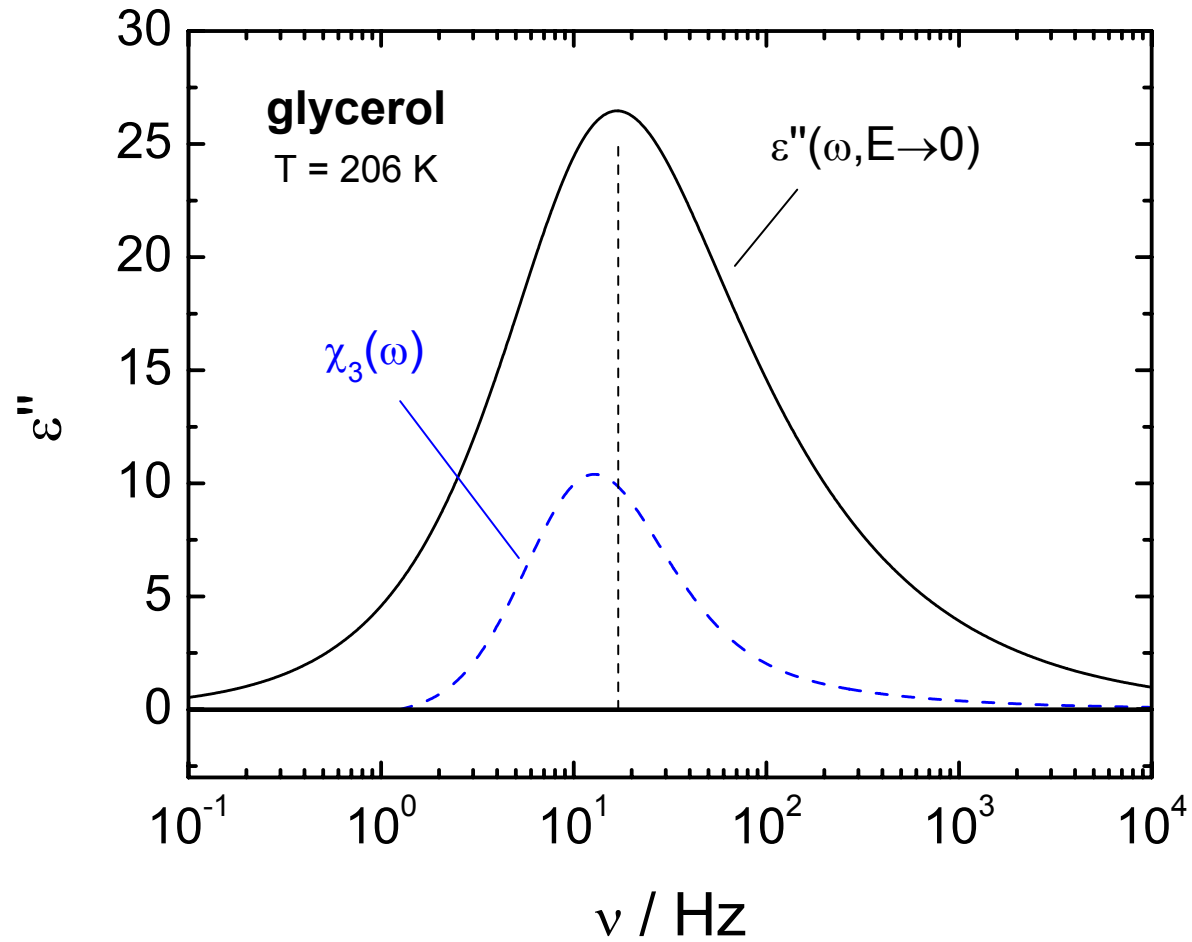
$$\Rightarrow A_\omega \approx \varepsilon \varepsilon_0 E_0$$

$$D_{3\omega}(t) = -\lambda \varepsilon \varepsilon_0 E_0^3 \frac{1}{4} \sin(3\omega t)$$

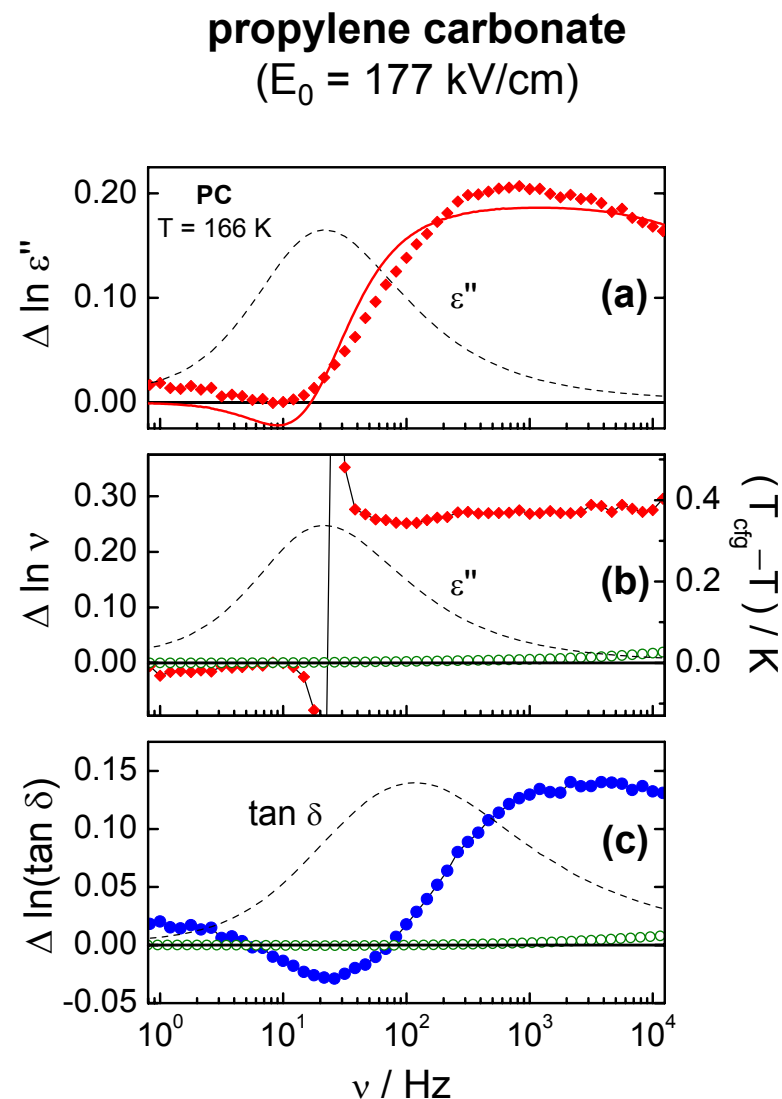
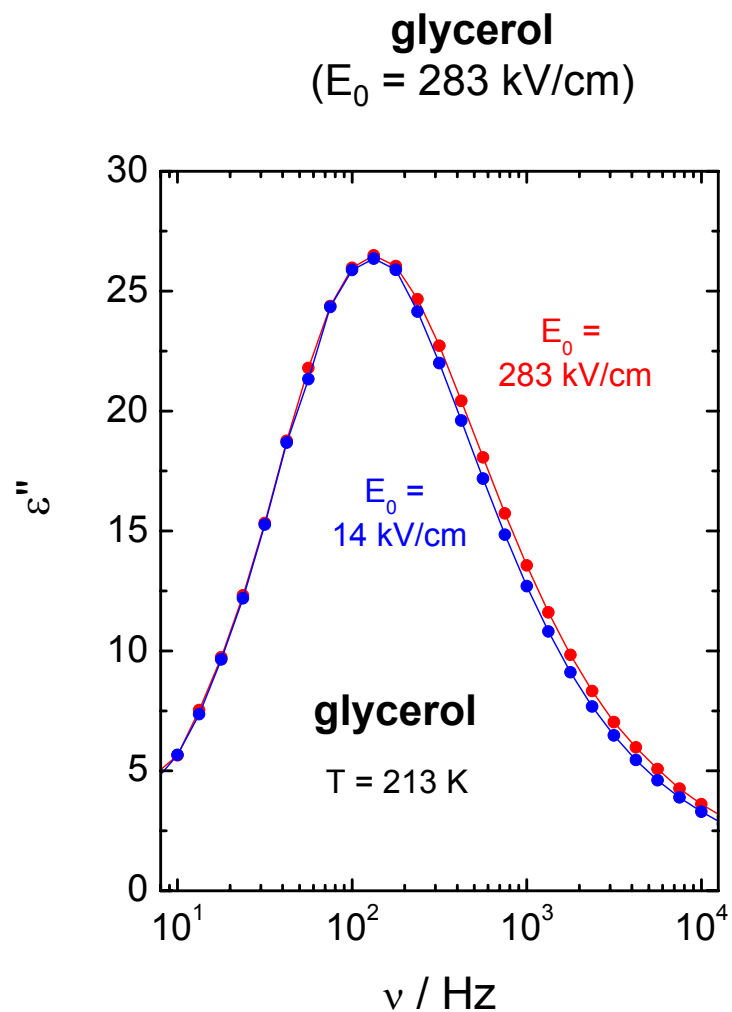
$$\Rightarrow A_{3\omega} = \frac{1}{4} \varepsilon \varepsilon_0 E_0 \Delta \ln \varepsilon$$

$$\frac{A_{3\omega}}{A_\omega} = \frac{\Delta \ln \varepsilon}{4}$$

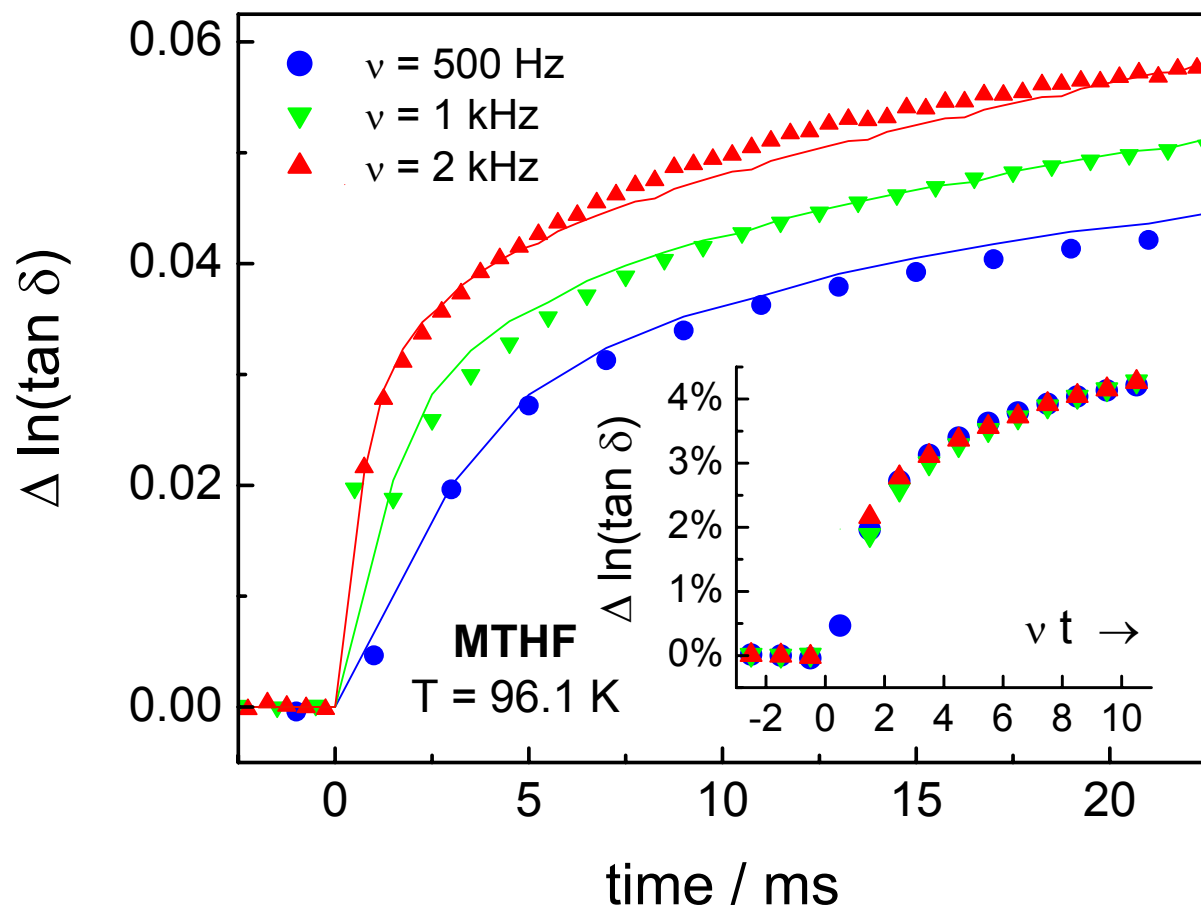
calculated frequency dependence of χ_3



high field impedance of glycerol and propylene carbonate

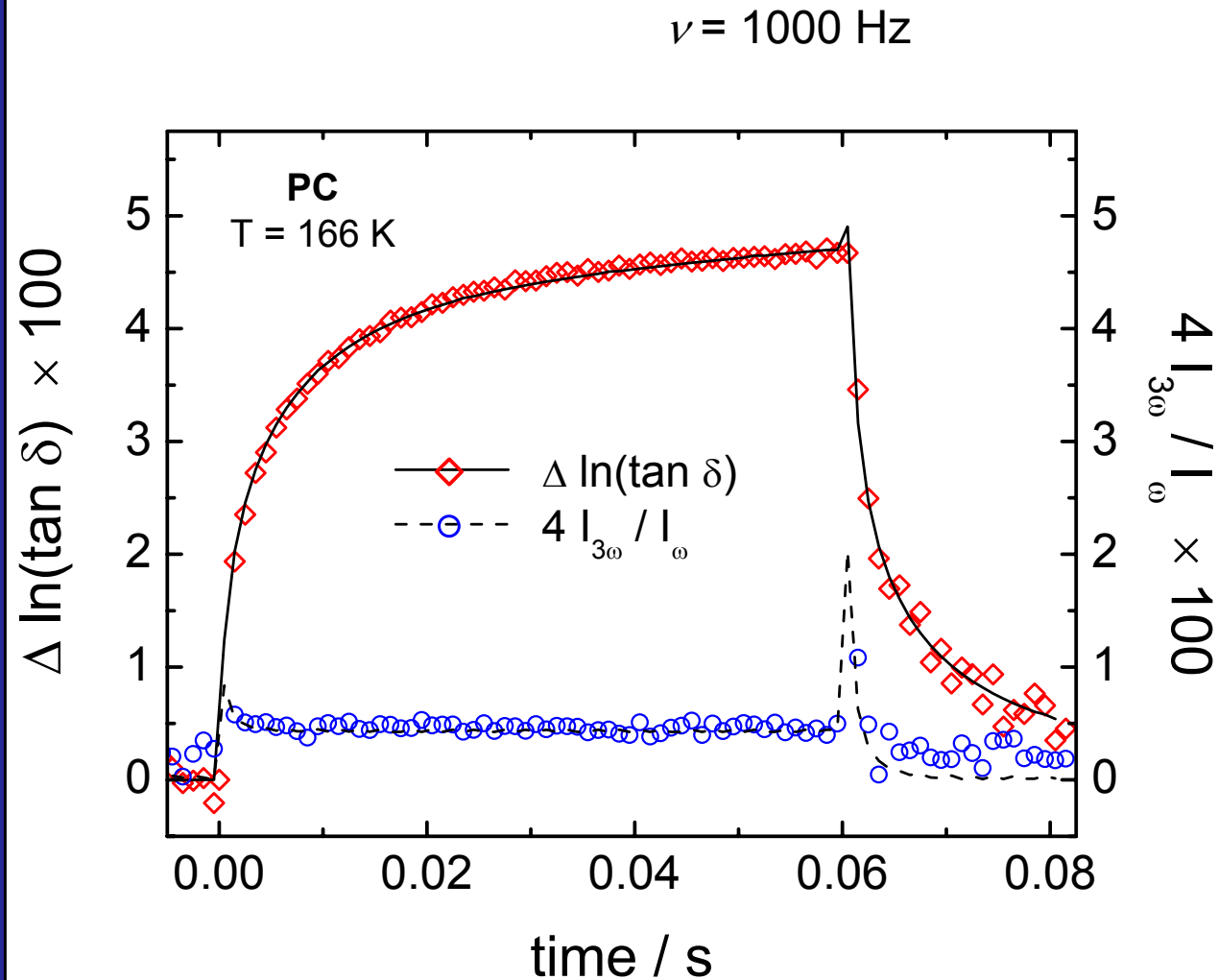


rise of configurational temperature for different frequencies



hallmark of
heterogeneity
regarding
 τ_T or $c_p(\omega)$

agreement between experiment and model



$$R = \frac{\omega}{\pi} \int_0^{2\pi/\omega} \sin(n\omega t) S(t) dt$$

$$I = \frac{\omega}{\pi} \int_0^{2\pi/\omega} \cos(n\omega t) S(t) dt$$

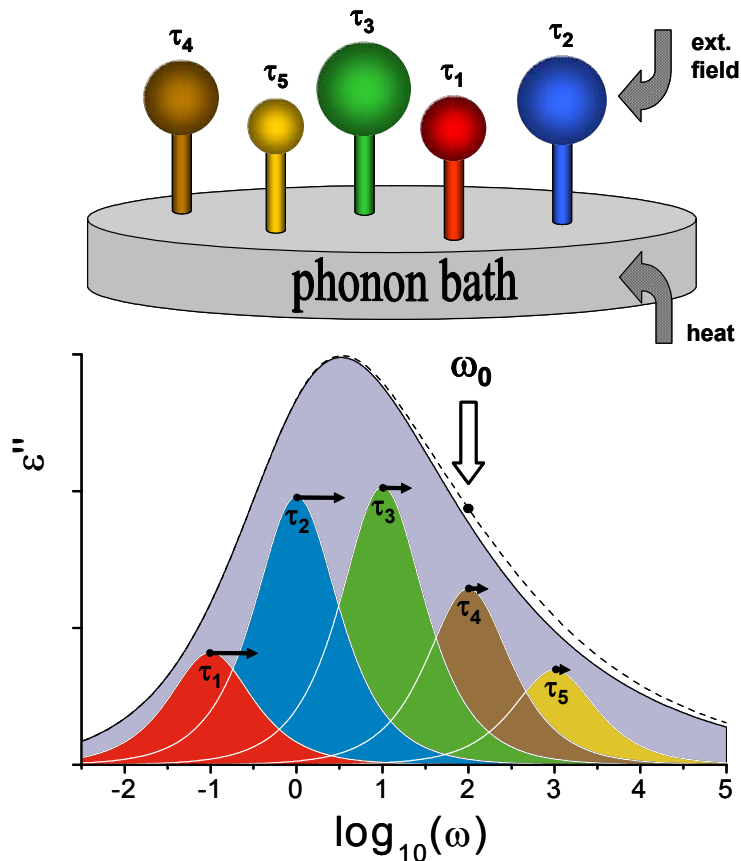
$$A = \sqrt{R^2 + I^2}$$

$$\varphi = \arctan\left(\frac{I}{R}\right)$$

$$\tan \delta = \tan\left(\frac{\pi}{2} - \Delta\varphi\right)$$

$$\frac{A_{3\omega}}{A_{\omega}} = \frac{\Delta \ln \varepsilon}{4}$$

non-steady state version of 'box'-model



separately for each domain i

$$\Delta \varepsilon_i = \Delta \varepsilon g(\tau) d\tau \Rightarrow \sum_i \Delta \varepsilon_i = \Delta \varepsilon$$

$$\Delta C_{p,i} = \Delta C_p g(\tau) d\tau \Rightarrow \sum_i \Delta C_{p,i} = \Delta C_p$$

initial conditions :

$$D_i(0) = 0 \text{ and } T_i(0) = T$$

$$\frac{dD_i(t)}{dt} = j_i(t) = \frac{\varepsilon_0 E(t) \Delta \varepsilon_i}{\tau_i(t)} - \frac{D_i(t)}{\tau_i(t)}$$

$$\frac{dT_i(t)}{dt} = \frac{j_i^2(t) \tau_i(t) V}{\varepsilon_0 \Delta \varepsilon_i \Delta C_{p,i}} - \frac{T_i(t) - T}{\tau_i(t)}$$

$$\tau_i(t) = \tau_i(0) \left[1 - \frac{T_i(t) - T}{T} \left(\frac{E_A}{k_B T} \right) \right]$$

$$\frac{dT}{dt} = \sum_i \frac{T_i(t) - T}{\tau_i(t)} \frac{\Delta C_{p,i}}{C_{p,\infty}} \text{ for adiabatic case}$$

$$V(t) = E(t) d$$

$$I(t) = A j_\infty + A \sum j_i(t) = A \left(\varepsilon_0 \varepsilon_\infty \frac{dE(t)}{dt} + \sum j_i(t) \right)$$

non-steady state version of 'box'-model

$$E(t) = E_0 \sin(\omega t)$$

for each mode 'i'

$$\Delta \varepsilon_i = \Delta \varepsilon g(\tau) d\tau \Rightarrow \sum_i \Delta \varepsilon_i = \Delta \varepsilon$$

$$\Delta C_{p,i} = \Delta C_p g(\tau) d\tau \Rightarrow \sum_i \Delta C_{p,i} = \Delta C_p$$

initial conditions : $D_i(0) = 0$ and $T_i(0) = T$ (equil.)

polarization :

$$\frac{dD_i(t)}{dt} = j_i(t) = \frac{\varepsilon_0 E(t) \Delta \varepsilon_i}{\tau_i(t)} - \frac{D_i(t)}{\tau_i(t)}$$

conf .temp.:

$$\frac{dT_i(t)}{dt} = + \frac{j_i^2(t) \tau_i(t) V}{\varepsilon_0 \Delta \varepsilon_i \Delta C_{p,i}} - \frac{T_i(t) - T}{\tau_i(t)}$$

adj. time const.:

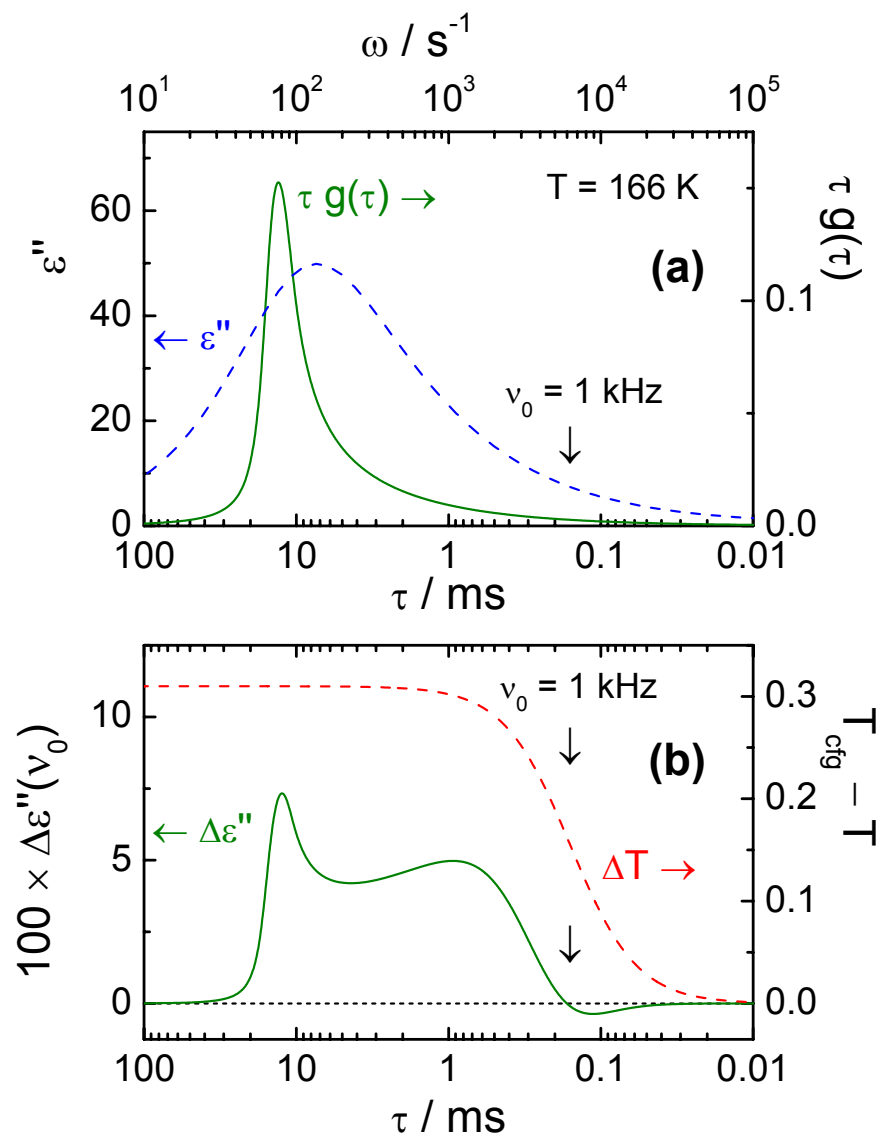
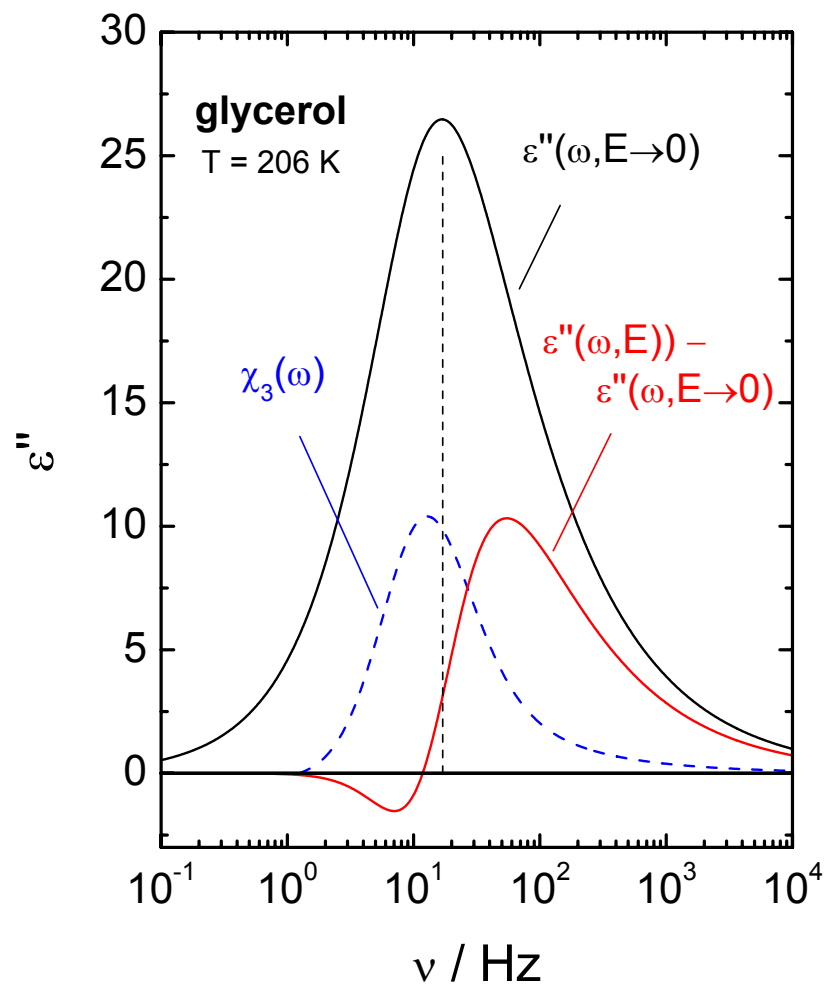
$$\tau_i(t) = \tau_i(0) \left[1 - \frac{T_i(t) - T}{T} \left(\frac{E_A}{k_B T} \right) \right]$$

$$V(t) = E(t) d$$

$$I(t) = A j_\infty + A \sum j_i(t)$$

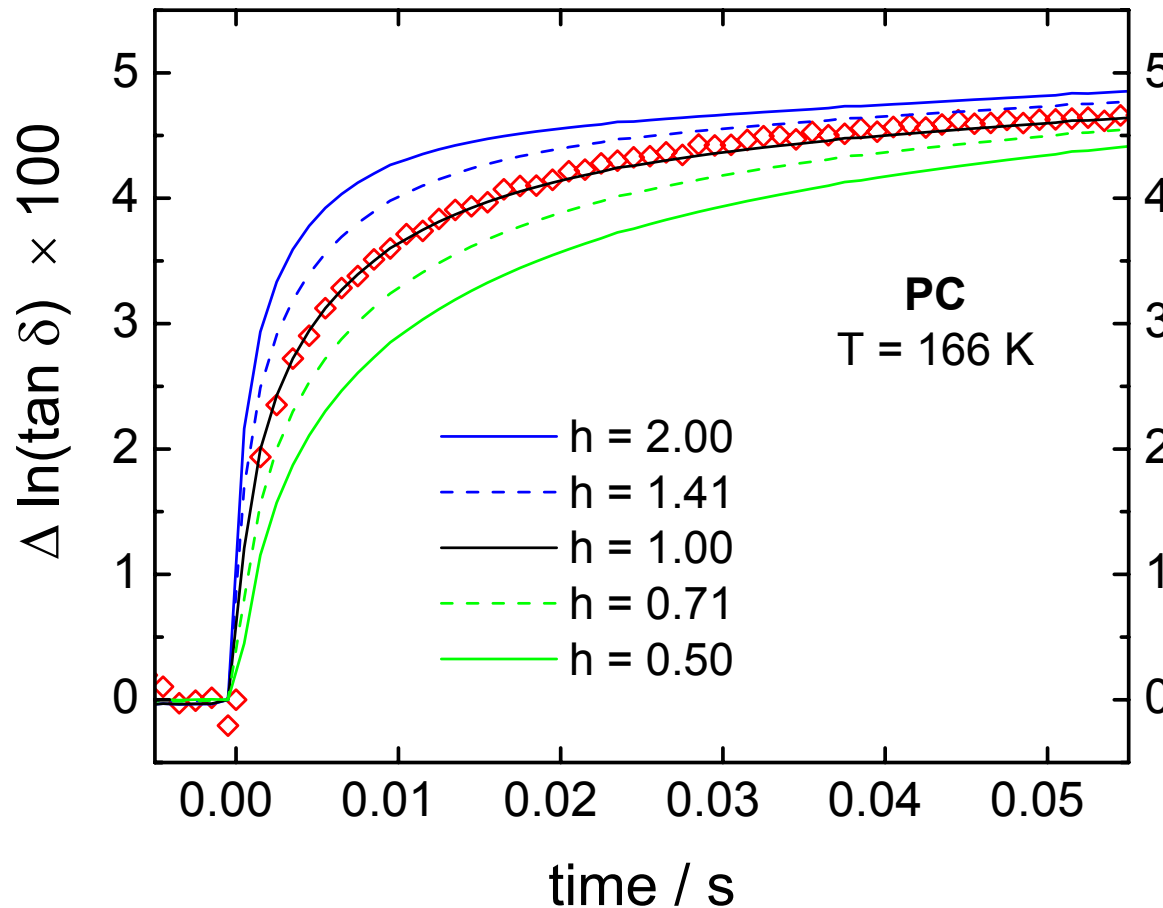
$$= A \left(\varepsilon_0 \varepsilon_\infty \frac{dE(t)}{dt} + \sum j_i(t) \right)$$

high field impedance technique



testing the claim: $\tau_T = \tau_D$ versus $\tau_T = \tau_D/h$

$$\ln \tau_D^* = \ln \tau_D - \frac{E_A}{k_B T^2} \times \frac{\varepsilon_0 E_0^2 \Delta \varepsilon}{2 \rho \Delta c_p} \times \frac{\omega^2 \tau_D \tau_T}{1 + \omega^2 \tau_D^2} \left[1 - e^{-\frac{t}{\tau_T}} \right] = \ln \tau_D - \frac{E_A}{k_B T^2} \times \frac{\varepsilon_0 E_0^2 \Delta \varepsilon}{2 \rho \Delta c_p / h} \times \frac{\omega^2 \tau_D \tau_D / h}{1 + \omega^2 \tau_D^2} \left[1 - e^{-\frac{t}{\tau_D / h}} \right]$$

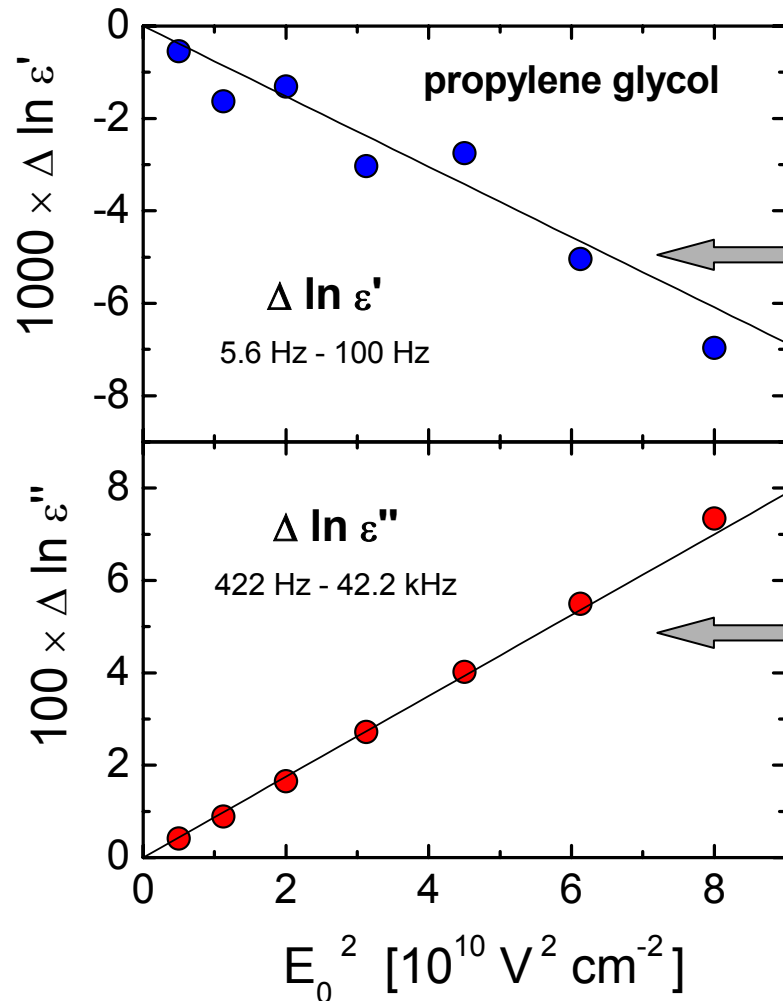


$$\tau_T \rightarrow \tau_D / h$$

result:

$$\tau_T = \tau_D \pm 15\%$$

summary of relevant non-linear effects ($\sim E^2$)



Coulombic stress :

$$Fd = \frac{1}{2} QV, Q = CV, C = \epsilon \epsilon_0 A/d$$

$$F(t) = \frac{\epsilon_s \epsilon_0 A}{2} E^2(t) = \underbrace{\frac{\epsilon_s \epsilon_0 A}{4} E_0^2}_{\approx 31 \text{ N}} - \frac{\epsilon_s \epsilon_0 A}{4} E_0^2 \cos(2\omega t)$$

dielectric saturation :

$$\frac{\Delta \epsilon_s}{E^2} = -\frac{N\mu^4}{45\epsilon_0 V(kT)^3} \times \frac{\epsilon_s^4 (\epsilon_\infty + 2)^4}{(2\epsilon_s + \epsilon_\infty)^2 (2\epsilon_s^2 + \epsilon_\infty^2)}$$

(van Vleck)

energy absorption :

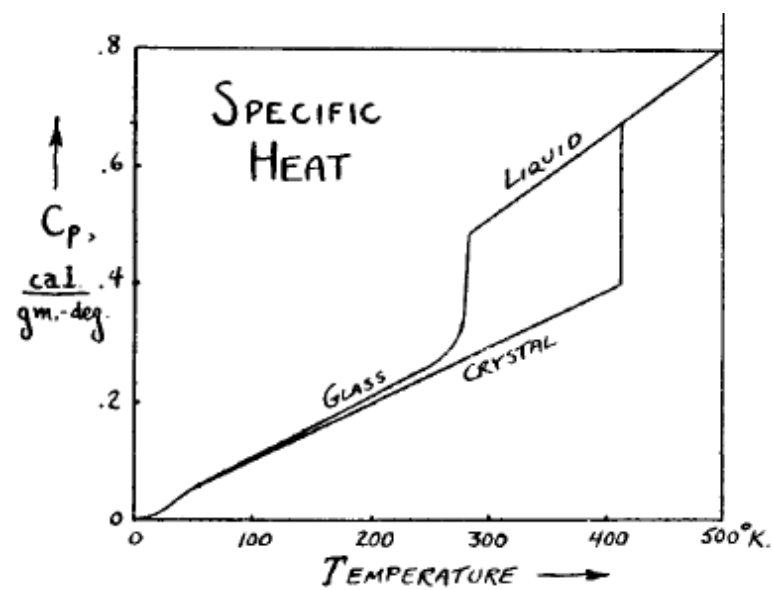
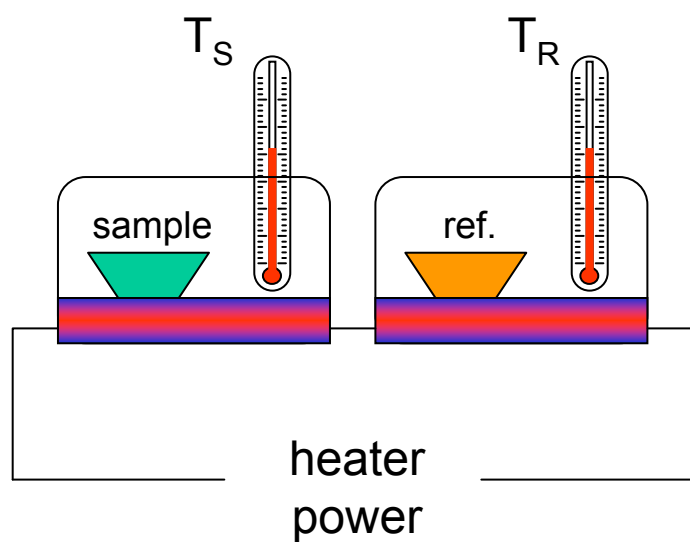
$$T_e(\tau) = \frac{\epsilon_0 E_0^2 \Delta \epsilon}{2\Delta c_p} \times \frac{\omega_0^2 \tau^2}{1 + \omega_0^2 \tau^2} = T_e^0 \times \frac{\omega_0^2 \tau^2}{1 + \omega_0^2 \tau^2}$$

$$\hat{\epsilon}(\omega) = \epsilon_\infty + \Delta \epsilon \int_0^\infty g(\tau) \frac{1}{1 + i\omega\tau^*} d\tau$$

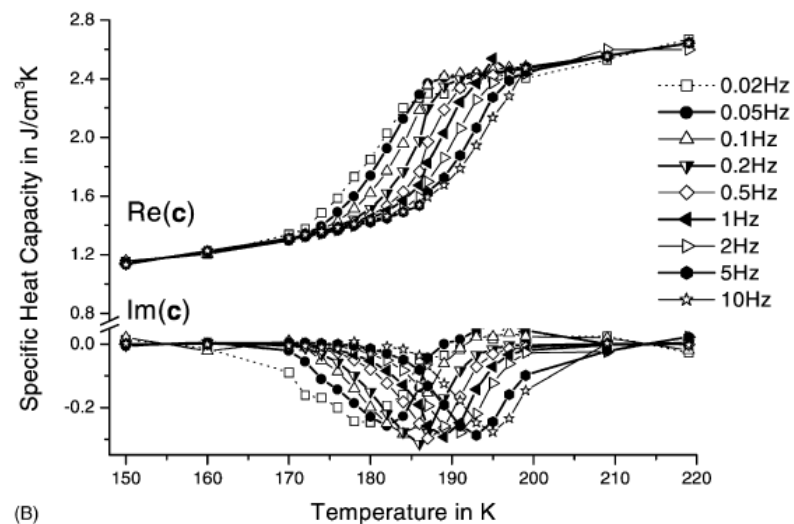
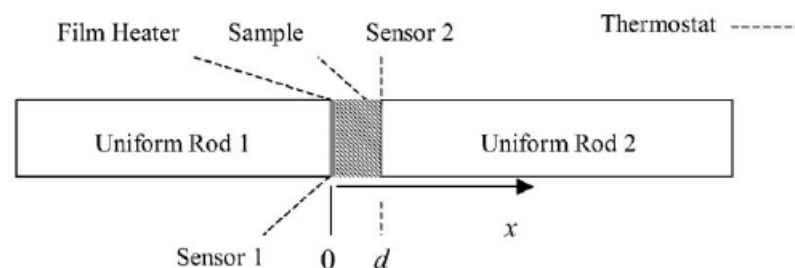
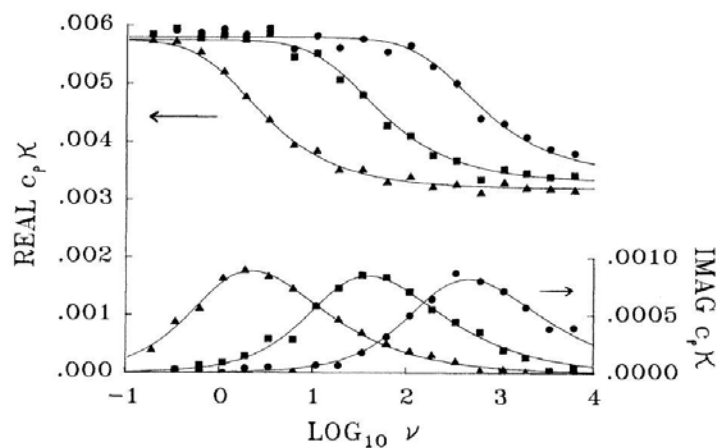
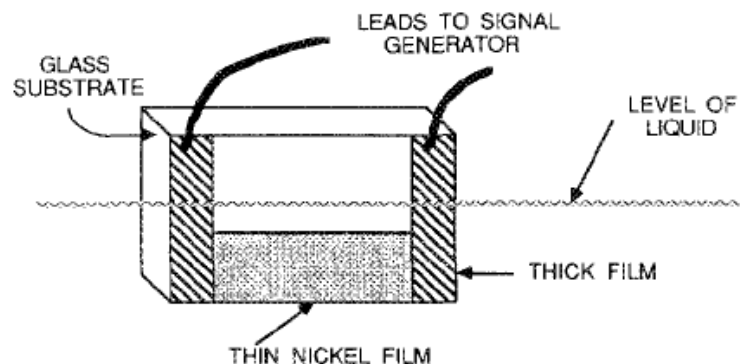
reverse calorimetry

basic techniques: heat capacity

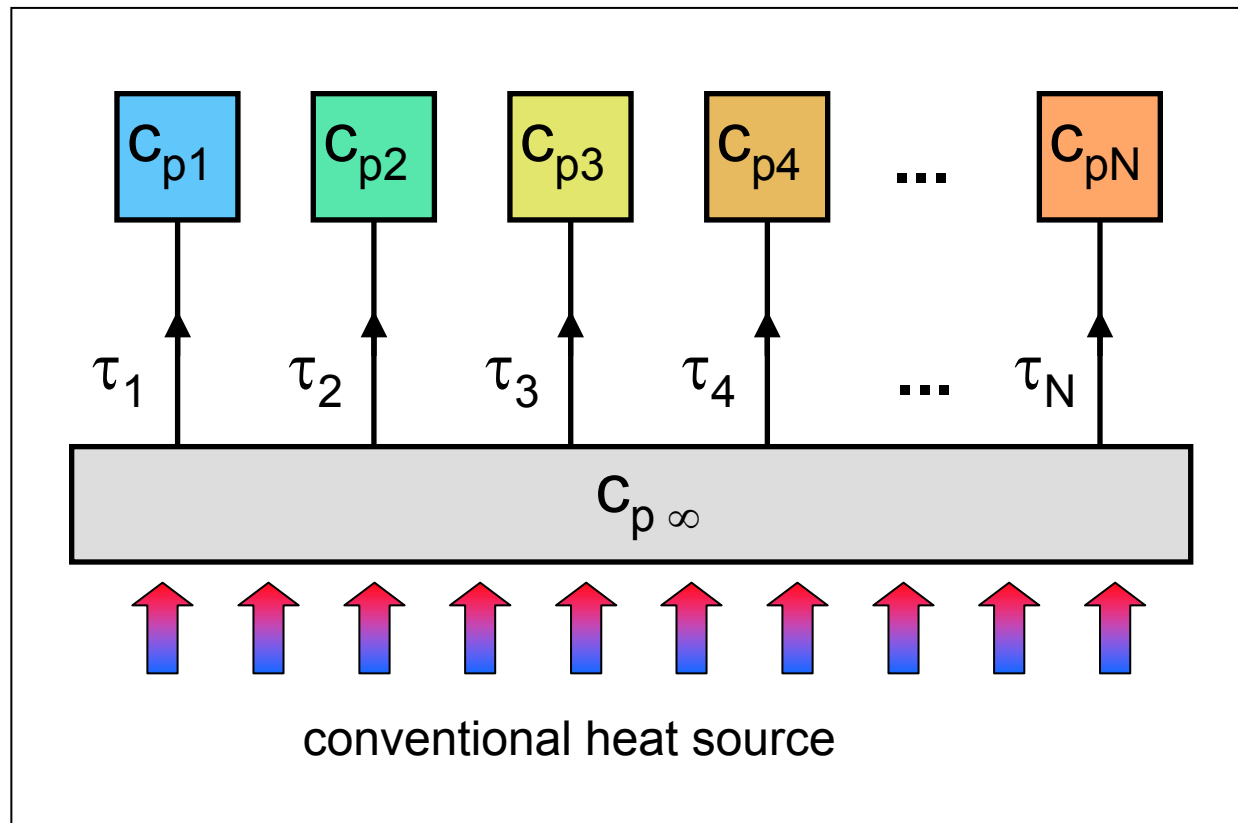
Differential Scanning Calorimetry



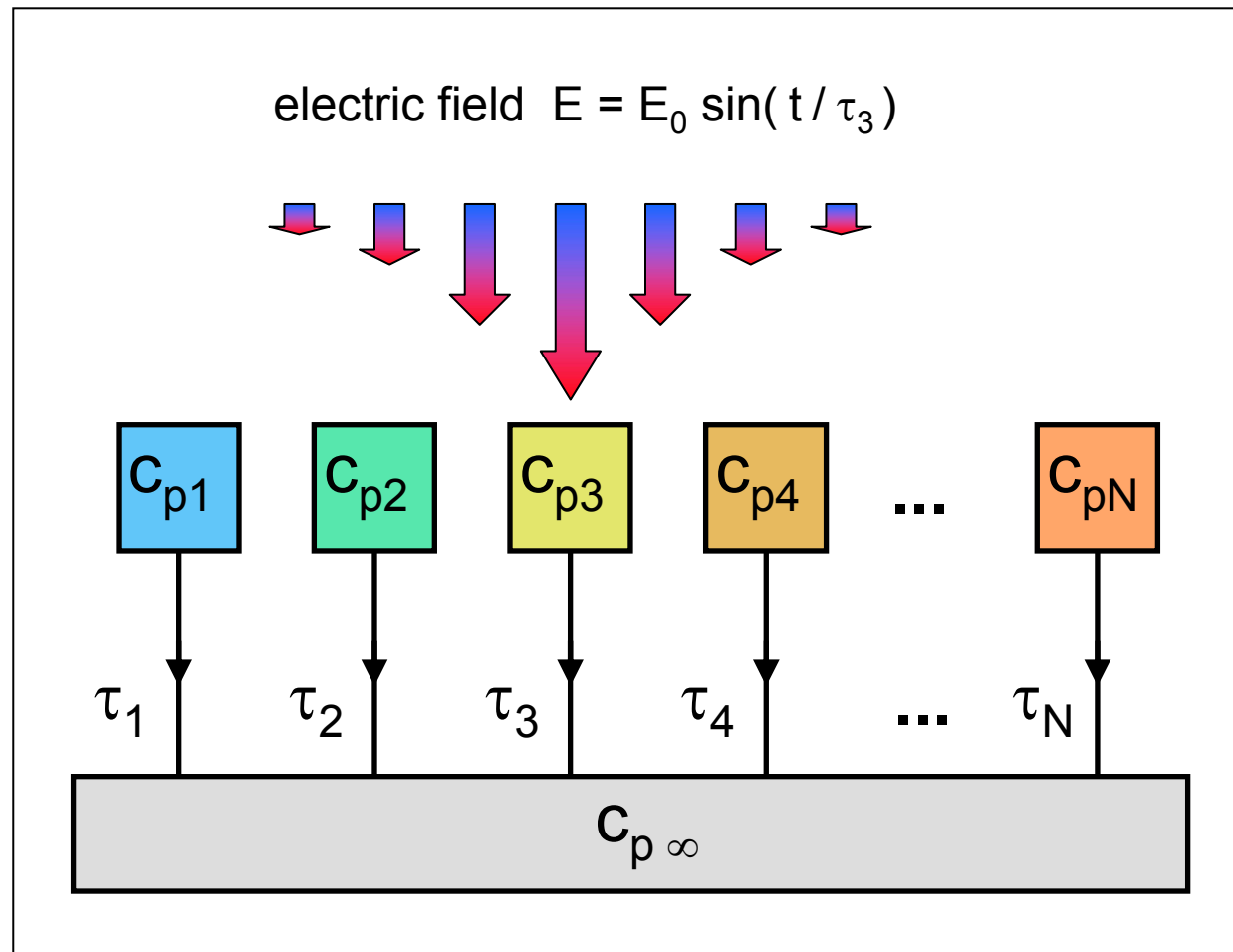
dynamic heat capacity in glycerol



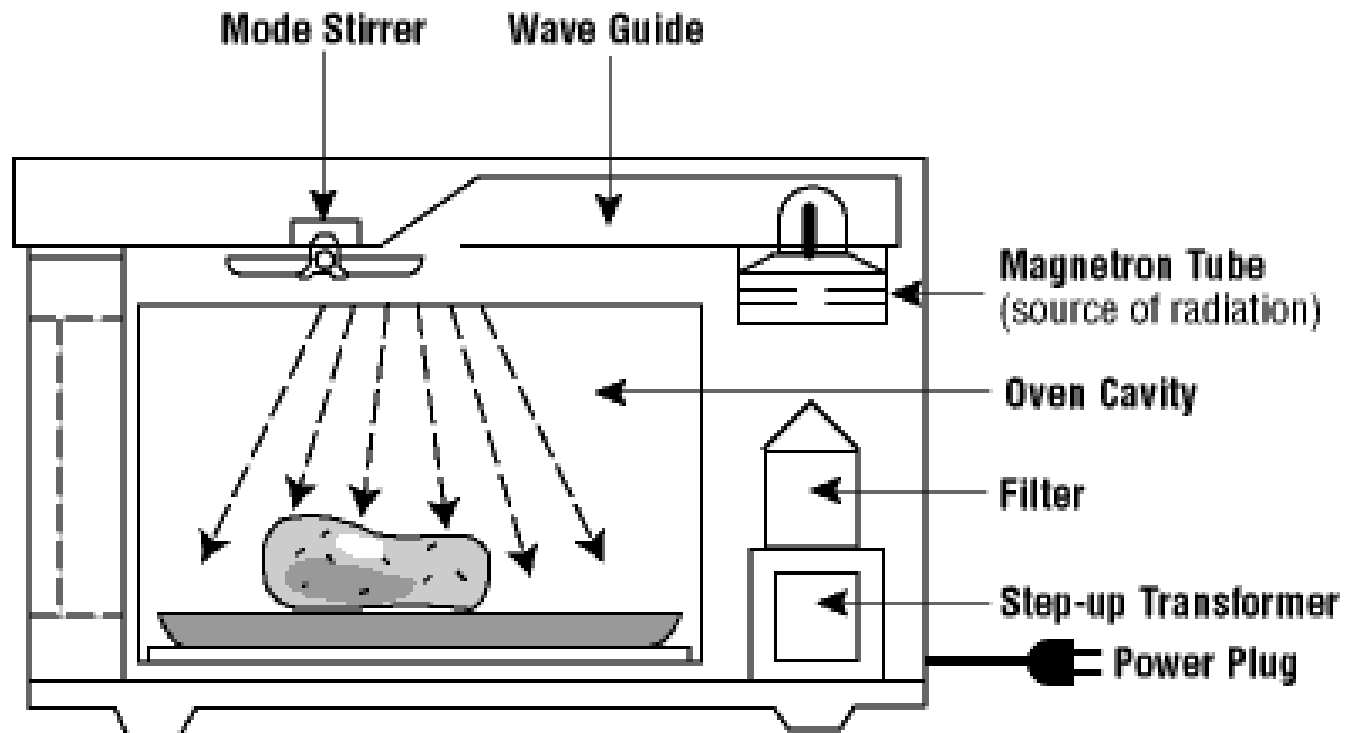
standard dynamic heat capacity



reverse dynamic heat capacity (isothermal)



reverse dynamic: microwave heating in slow motion



typical frequency: 2.45 GHz

what do we learn ?

nonlinearity from energy absorption
measure configurational C_p
thermal time scales
thermal heterogeneity
alcohols / ionic liquids
physical aging